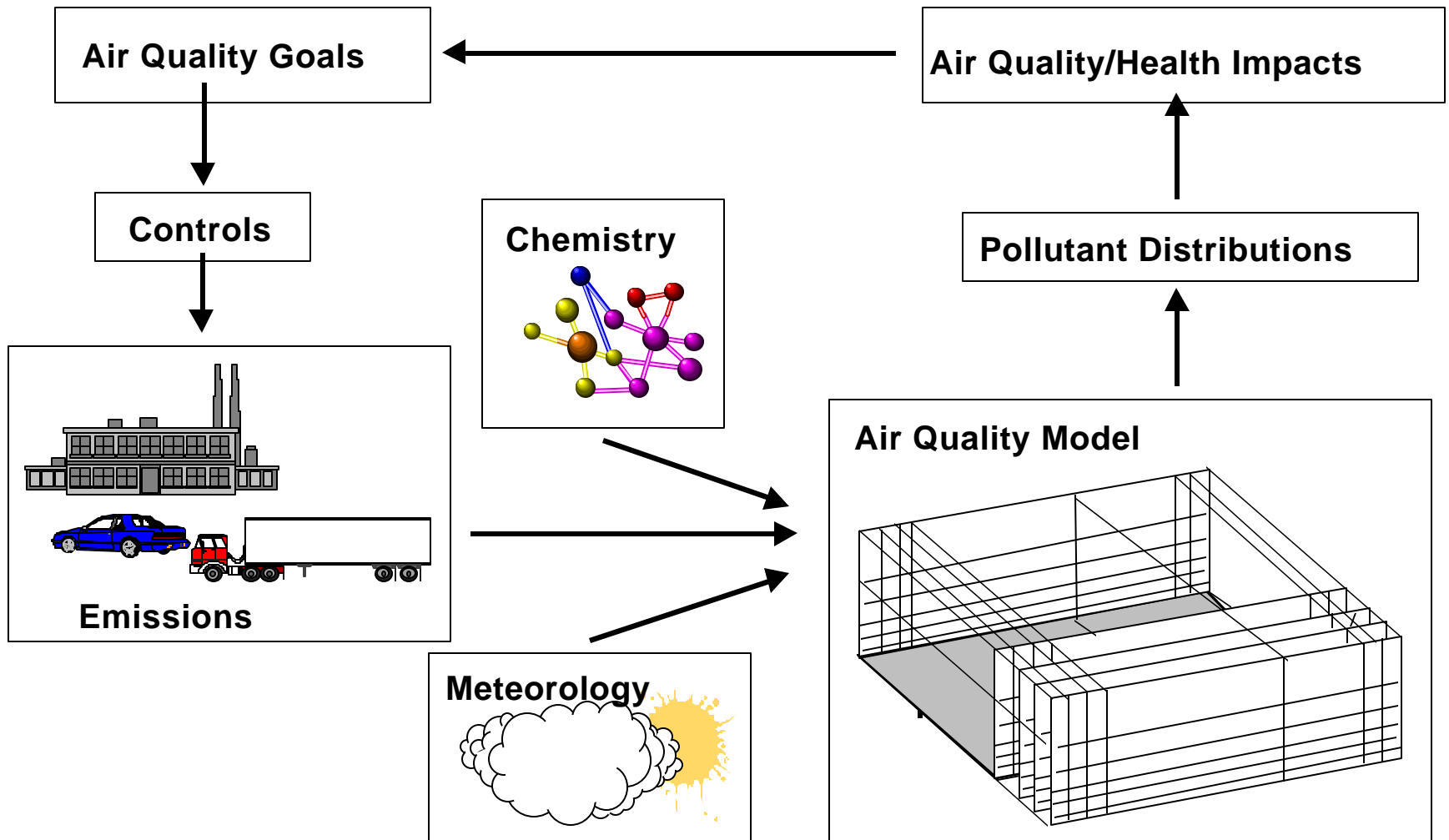


*Non-linearity in Atmospheric Response:
A Sensitivity Analysis Approach
Using
High-Order Decoupled Direct Method (HDDM)*

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Air quality modeling



Air quality modeling (contd.)



- Air quality models are indispensable part of air quality management.
 - The main tool to evaluate the effectiveness of different control strategies.
- They possess more information than we generally use.
 - Local sensitivity coefficients, i.e. derivatives.
 - More dimensions to look at.
- First-order sensitivity analysis does not capture nonlinearities.
 - Viewed as limitation.
- A high-order sensitivity analysis technique is developed.

The idea of sensitivity analysis



- How does the model respond to a change in an independent parameter?
 - Almost any modeling practice is, in essence, an effort to address this question directly or indirectly.
- In air quality modeling the sensitivity question is addressed directly to:
 - Quantify the atmospheric response to emissions control,
 - Find the uncertainty in the response,
 - Perform inverse modeling and data assimilation,
 - Etc.

Brute-force sensitivity analysis

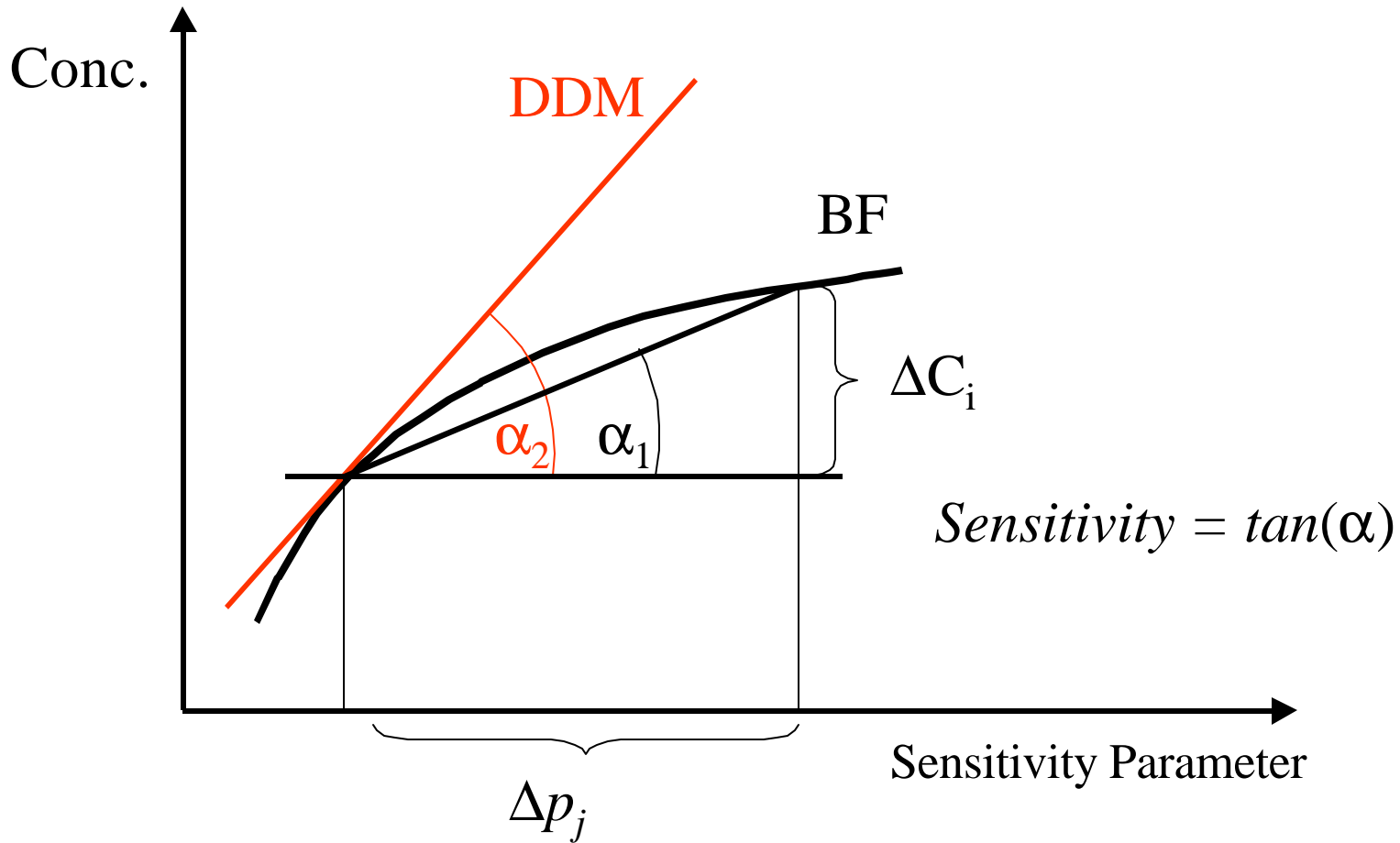


- Approximates the derivative as the sensitivity parameter approaches zero:

$$S_{ij} \cong \frac{\Delta C_i}{\Delta p_j}$$

- One-at-a-time perturbation of each sensitivity parameter.
- Pros and cons:
 - Easy to do,
 - One additional run for each additional sensitivity parameter,
 - Noisy for small perturbations,
 - Unrealistic for large perturbations.

Brute-force sensitivity analysis (contd.)



DDM sensitivity analysis

- Decoupled Direct Method (Dunker, 1981 and 1984): Sensitivity equations are derived and integrated decoupled from concentrations.
 - The only direct sensitivity technique that has been applied in 3-D air quality models [DDM-3D (Yang et al., 1997)],
 - Drawbacks of the brute-force sensitivity analysis avoided.

$$\begin{array}{l} \frac{\partial C_i}{\partial t} \\ \frac{\partial S_{ij}}{\partial t} \end{array} = \begin{array}{|l} \text{Advection} \\ -\nabla(\mathbf{u}C_i) \\ -\nabla(\mathbf{u}S_{ij}) \end{array} \begin{array}{|l} \text{Diffusion} \\ +\nabla(\mathbf{K}\nabla C_i) \\ +\nabla(\mathbf{K}\nabla S_{ij}) \end{array} \begin{array}{|l} \text{Chemistry} \\ +R_i \\ +\mathbf{J}\mathbf{S}_j \end{array} \begin{array}{|l} \text{Emissions} \\ +E_i \\ +E_i \end{array}$$

DDM: computational efficiency



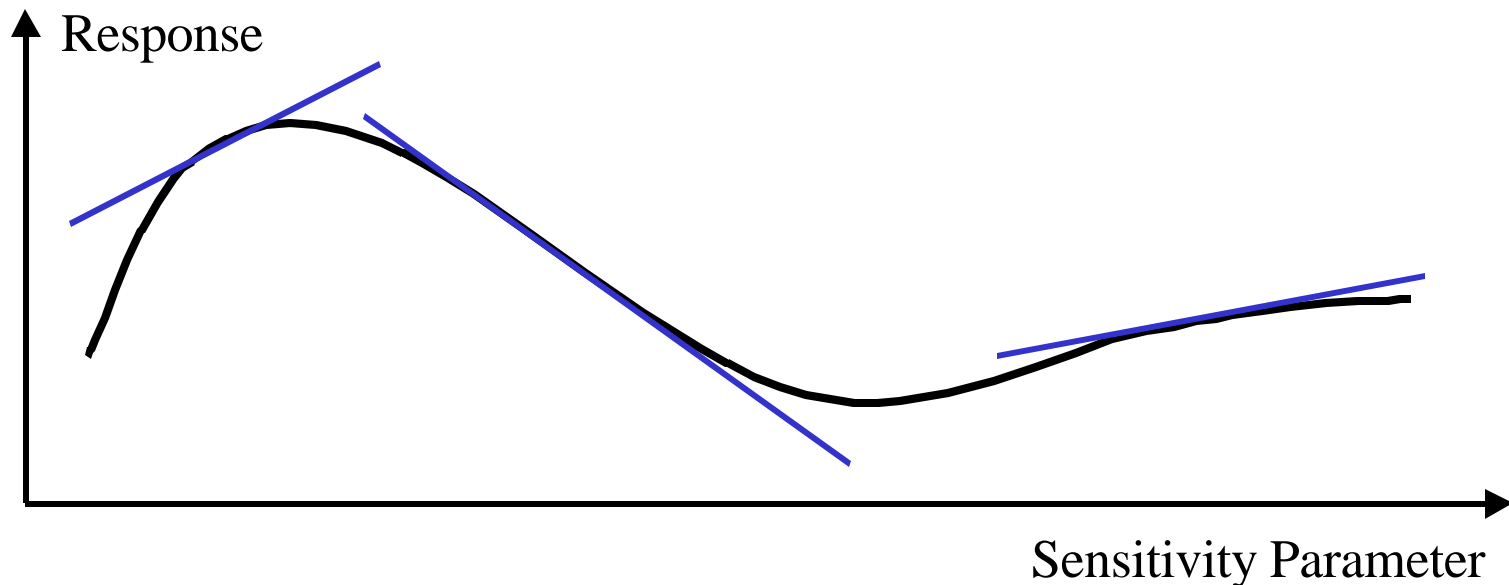
- DDM-3D is easy to implement because for the most part the same numerical routines are used to integrate the sensitivities.
- Chemistry discretization:

$$\mathbf{S}^{n+1} = \left(\mathbf{I} - \frac{\Delta t}{2} \mathbf{J}_c \right)^{-1} \left(\mathbf{I} + \frac{\Delta t}{2} \mathbf{J}_c \right) \mathbf{S}^n$$

- Matrix inversion is done only once for each grid cell and time step.

How to address non-linearity?

First-order sensitivity coefficients (slopes) cannot describe the non-linearities in the response -- 2nd order (curvature) or higher-order coefficients are required.



Calculation of higher-order derivatives

High-order Decoupled Direct Method (HDDM):

$$\frac{\partial S_{ij}^{(1)}}{\partial t} = -\nabla(\mathbf{u}S_{ij}^{(1)}) + \nabla(\mathbf{K}\nabla S_{ij}^{(1)}) + E_i + \mathbf{J}_i \mathbf{S}_j^{(1)}$$

$$\frac{\partial S_{ij}^{(2)}}{\partial t} = -\nabla(\mathbf{u}S_{ij}^{(2)}) + \nabla(\mathbf{K}\nabla S_{ij}^{(2)}) + \mathbf{J}_i \mathbf{S}_j^{(2)} + \mathbf{J}_{S^{(1)}}^* \mathbf{S}_j^{(1)}$$

$$\frac{\partial S_{ij}^{(m)}}{\partial t} = -\nabla(\mathbf{u}S_{ij}^{(m)}) + \nabla(\mathbf{K}\nabla S_{ij}^{(m)}) + \mathbf{J}_i \mathbf{S}_j^{(m)} + \sum_{k=1}^{m-1} \binom{m-1}{k} \mathbf{J}_{S^{(k)}}^* \mathbf{S}_j^{(m-k)}$$

Calculation of higher-order derivatives (contd.)

Chemistry discretization in HDDM:

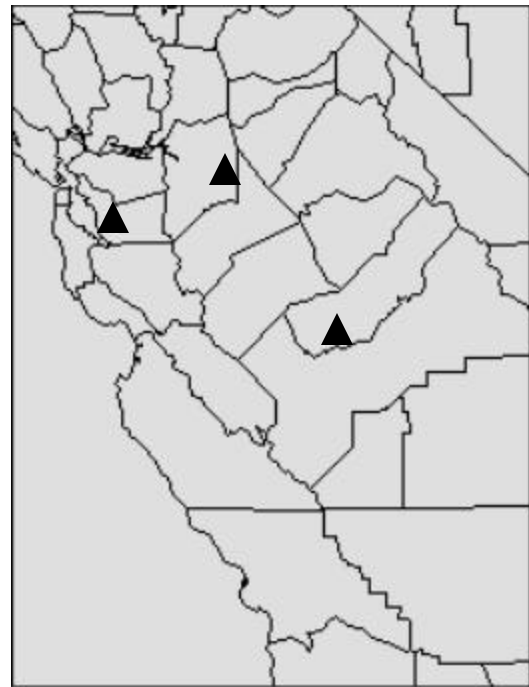
$$\mathbf{S}^{(1)^{n+1}} = \left(\mathbf{I} - \frac{\Delta t}{2} \mathbf{J}_c \right)^{-1} \left(\mathbf{I} + \frac{\Delta t}{2} \mathbf{J}_c \right) \mathbf{S}^{(1)^n}$$

$$\mathbf{S}^{(2)^{n+1}} = \left(\mathbf{I} - \frac{\Delta t}{2} \mathbf{J}_c \right)^{-1} \left[\left(\mathbf{I} + \frac{\Delta t}{2} \mathbf{J}_c \right) \mathbf{S}^{(2)^n} + \Delta t \mathbf{J}_{S^{(1)}}^* \mathbf{S}^{(1)} \right]$$

$$\mathbf{S}^{(m)^{n+1}} = \left(\mathbf{I} - \frac{\Delta t}{2} \mathbf{J}_c \right)^{-1} \left[\left(\mathbf{I} + \frac{\Delta t}{2} \mathbf{J}_c \right) \mathbf{S}^{(m)^n} + \Delta t \sum_{k=1}^{m-1} \binom{m-1}{k} \mathbf{J}_{S^{(k)}}^* \mathbf{S}^{(m-k)} \right]$$

Method test results

- Multiscale Air Quality Simulation Platform (MAQSIP)
 - Some modifications from the original model, inputs: e.g., BCs, mass conservation scheme,
 - Results shown for CB-IV, SAPRC-99 results to come soon.
- SARMAP modeling domain and episode (August 2-6, 1990).

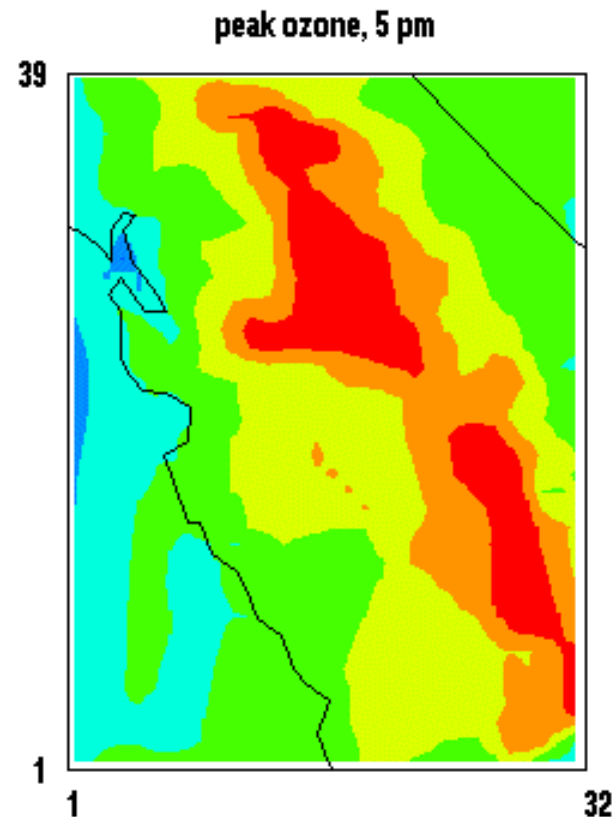
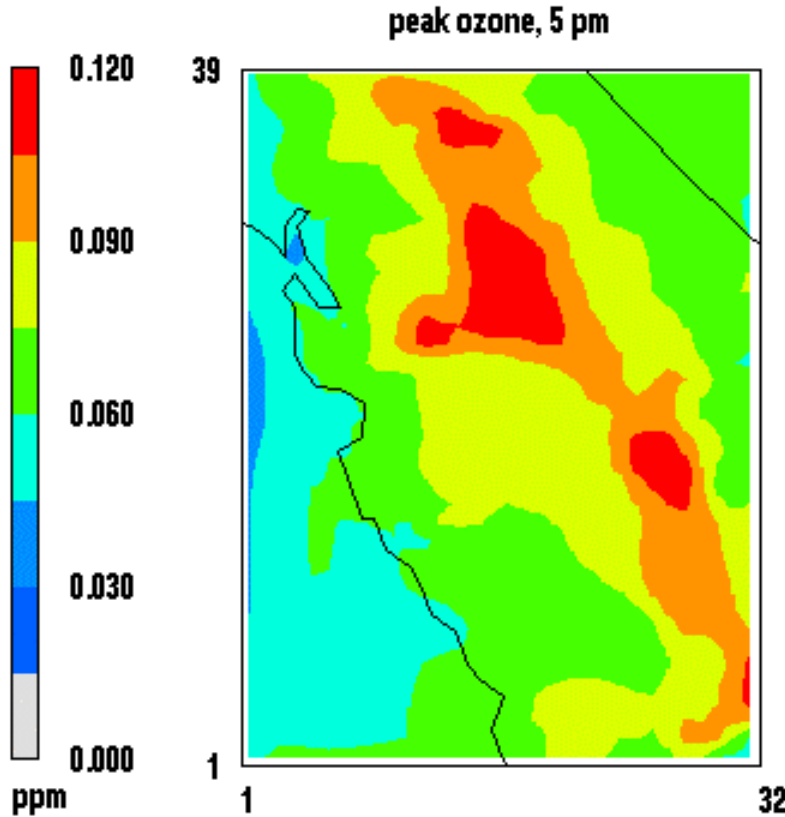


Simulated ozone: SAPRC-99 vs. CB-IV

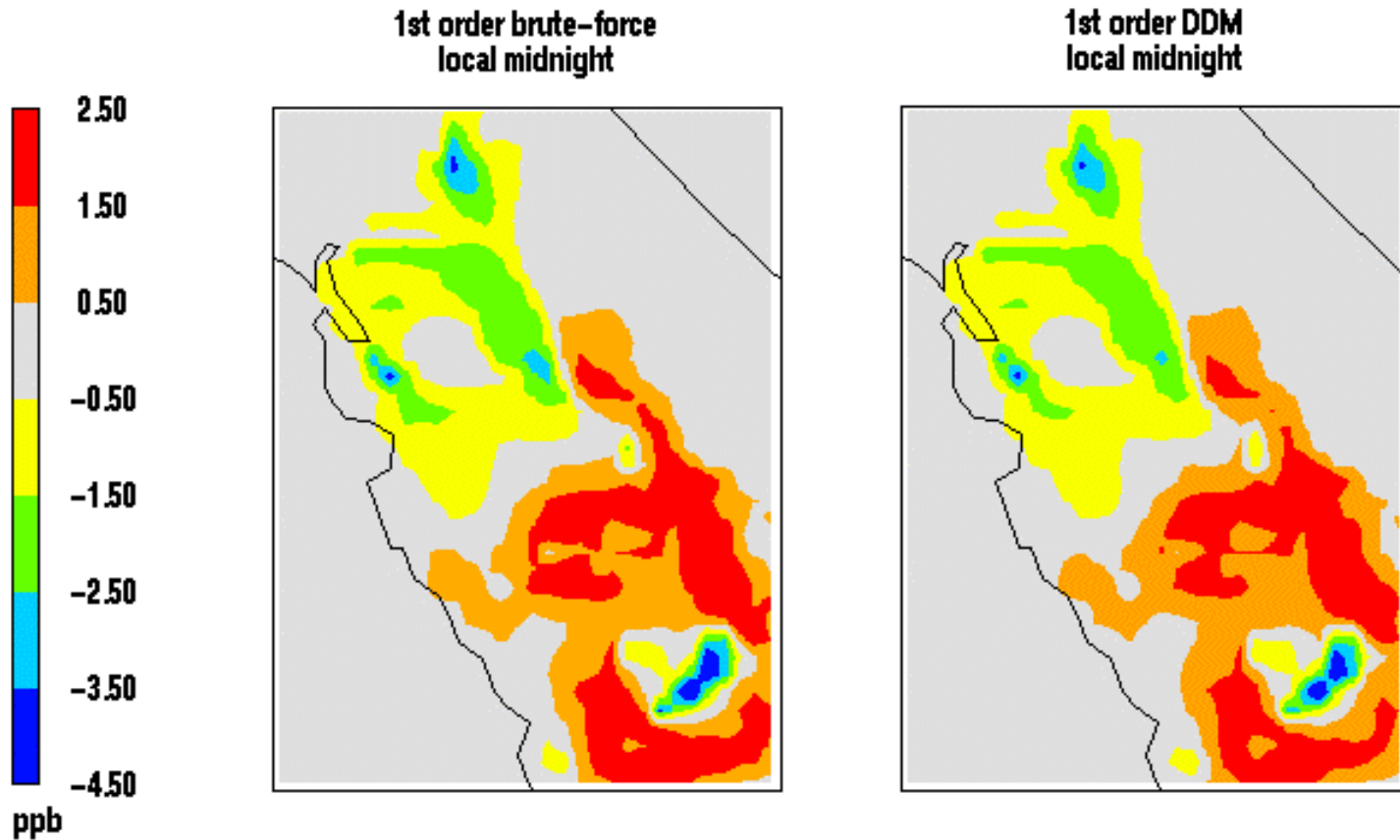


CB-IV

SAPRC-99

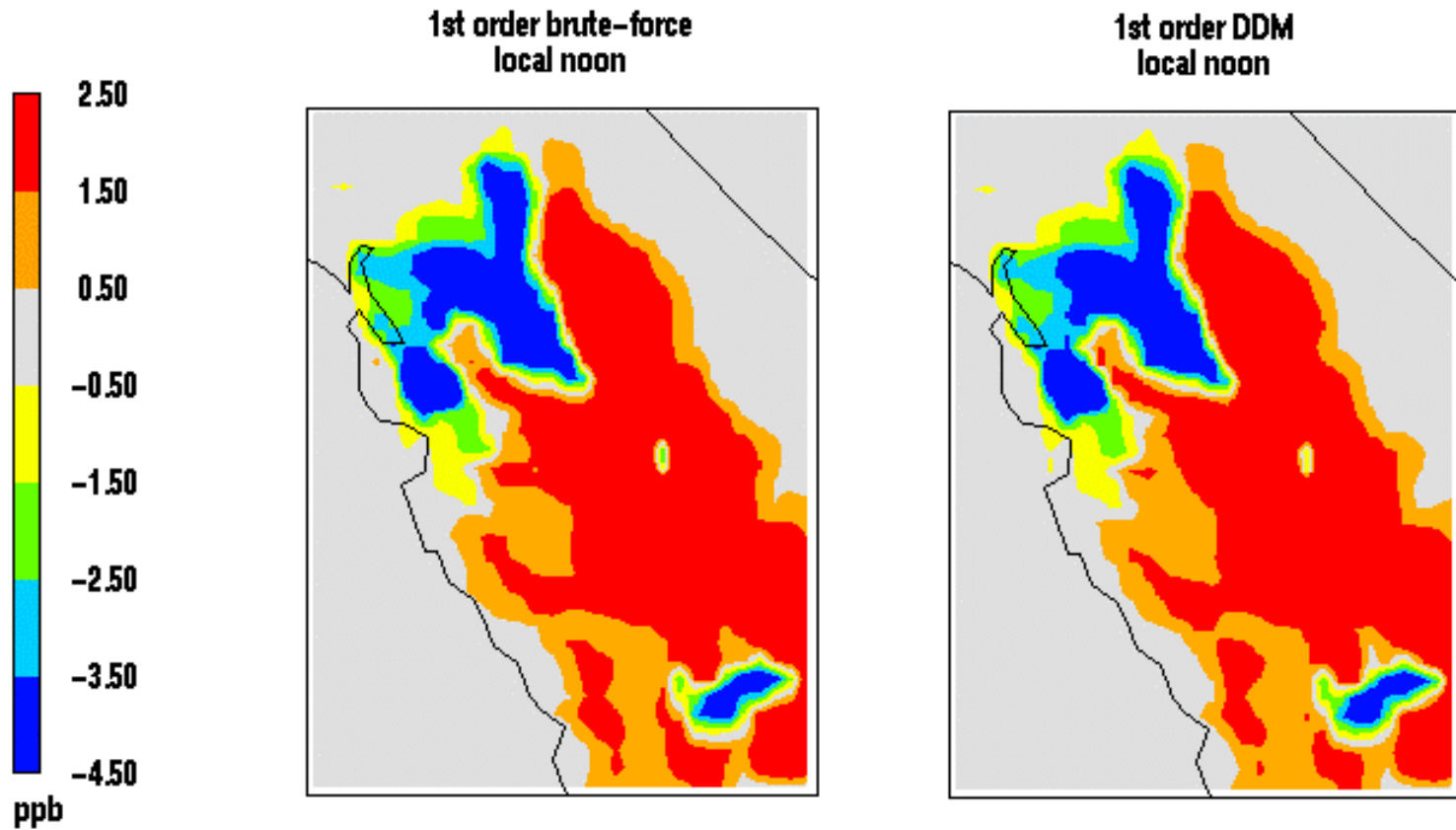


DDM vs. BF: 1st order derivative, midnight



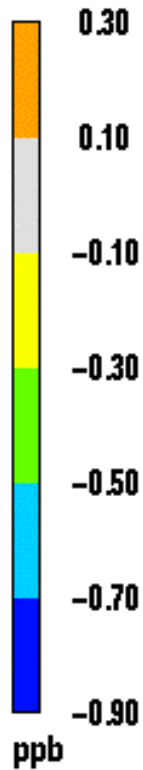
25% perturbation in domain-wide NO emissions

DDM vs. BF: 1st order derivative, noon

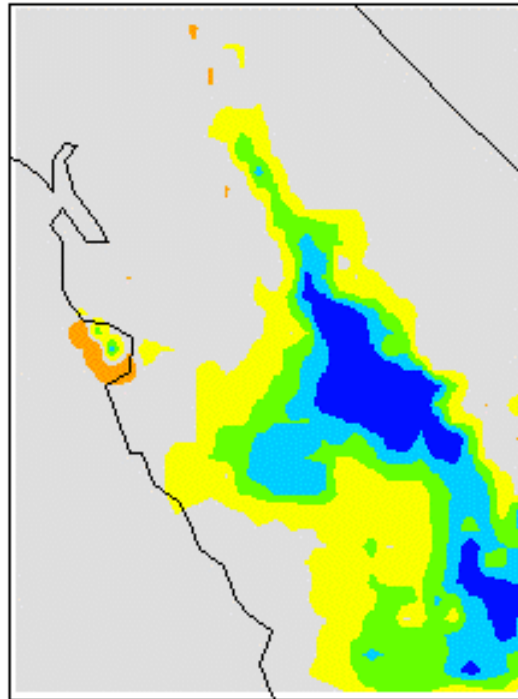


25% perturbation in domain-wide NO emissions

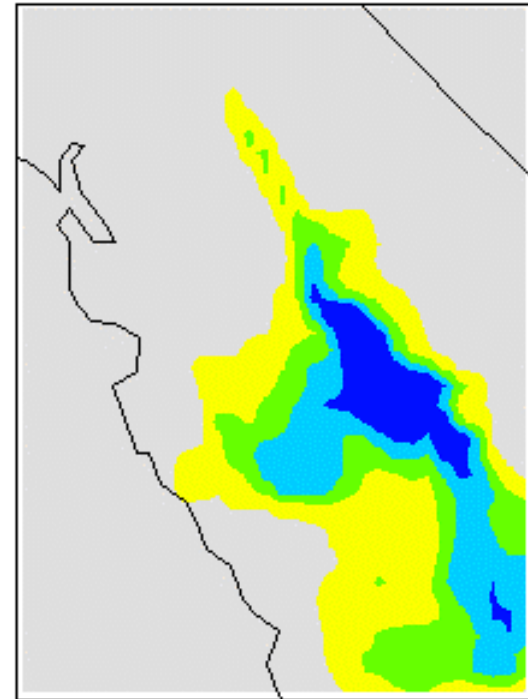
DDM vs. BF: 2nd order derivative, midnight



**Brute-force
local midnight**

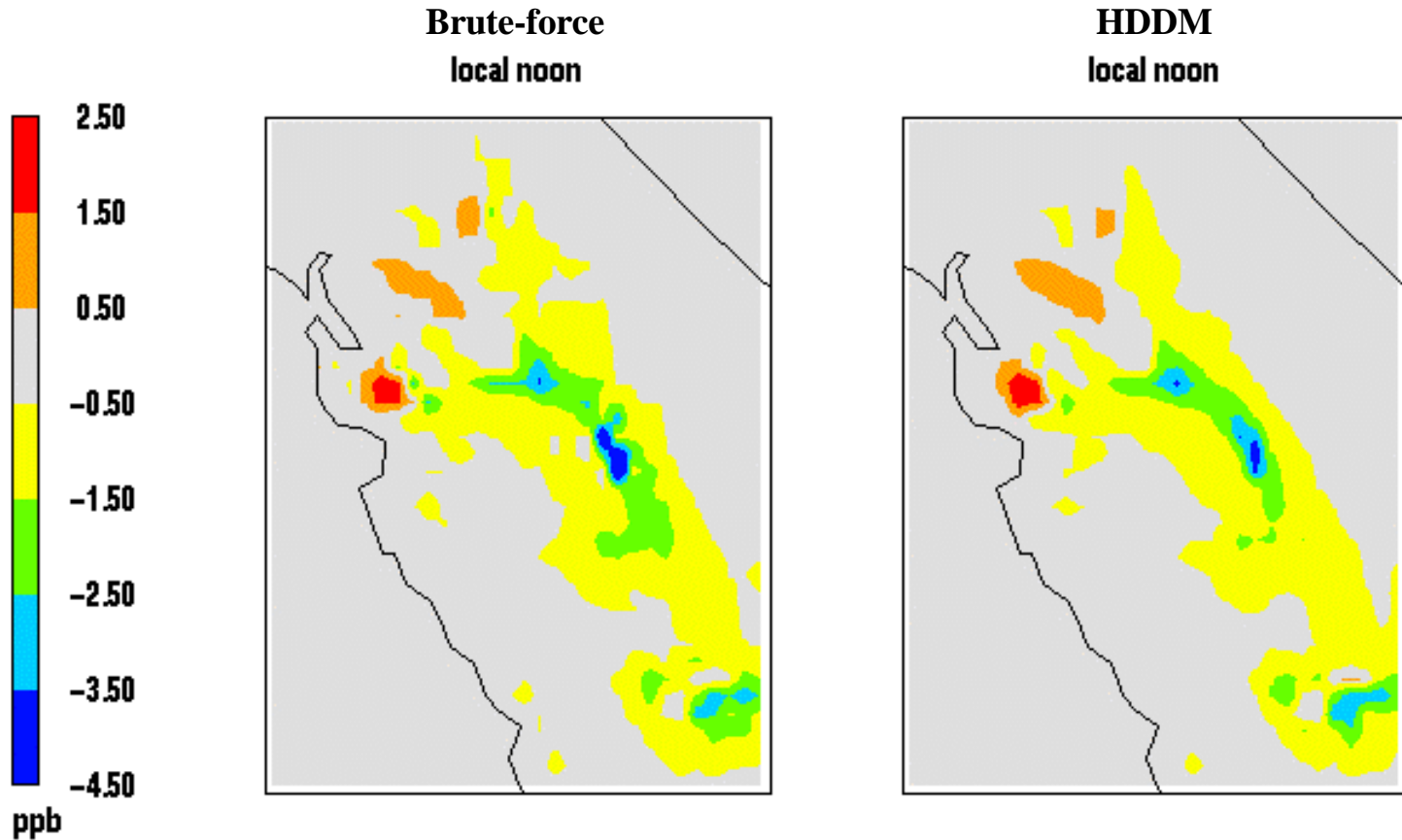


**HDDM
local midnight**



25% perturbation in domain-wide NO emissions

DDM vs. BF: 2nd order derivative, noon



25% perturbation in domain-wide NO emissions

DDM vs. BF?

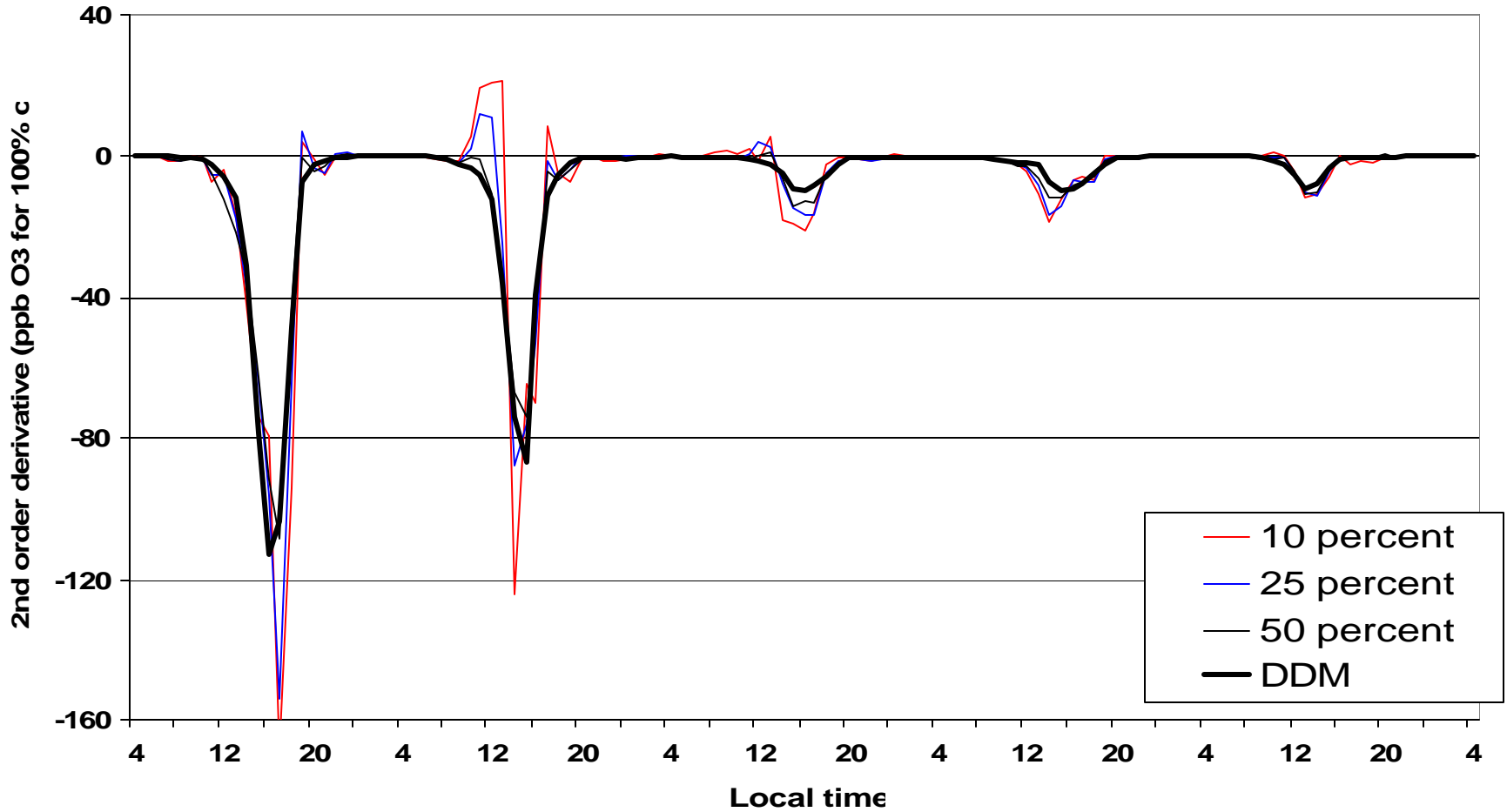


- Better agreement between BF and (H)DDM for the 1st order sensitivity coefficients than 2nd order:
 - 2nd order brute-force approximation is more susceptible to numerical noise.

$$S^{(1)} \cong \frac{C(p + \Delta p) - C(p - \Delta p)}{2\Delta p}$$

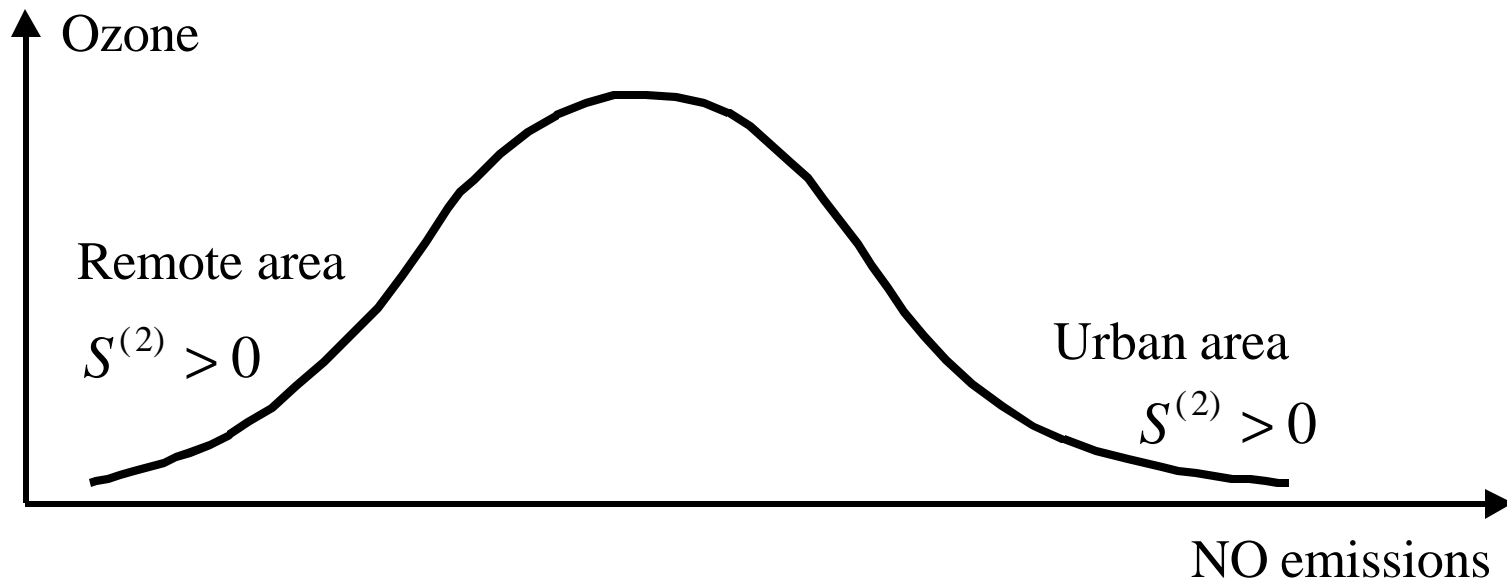
$$S^{(2)} \cong \frac{C(p + \Delta p) - 2C(p) + C(p - \Delta p)}{\Delta p^2}$$

DDM vs. BF 2nd order derivative: peak ozone

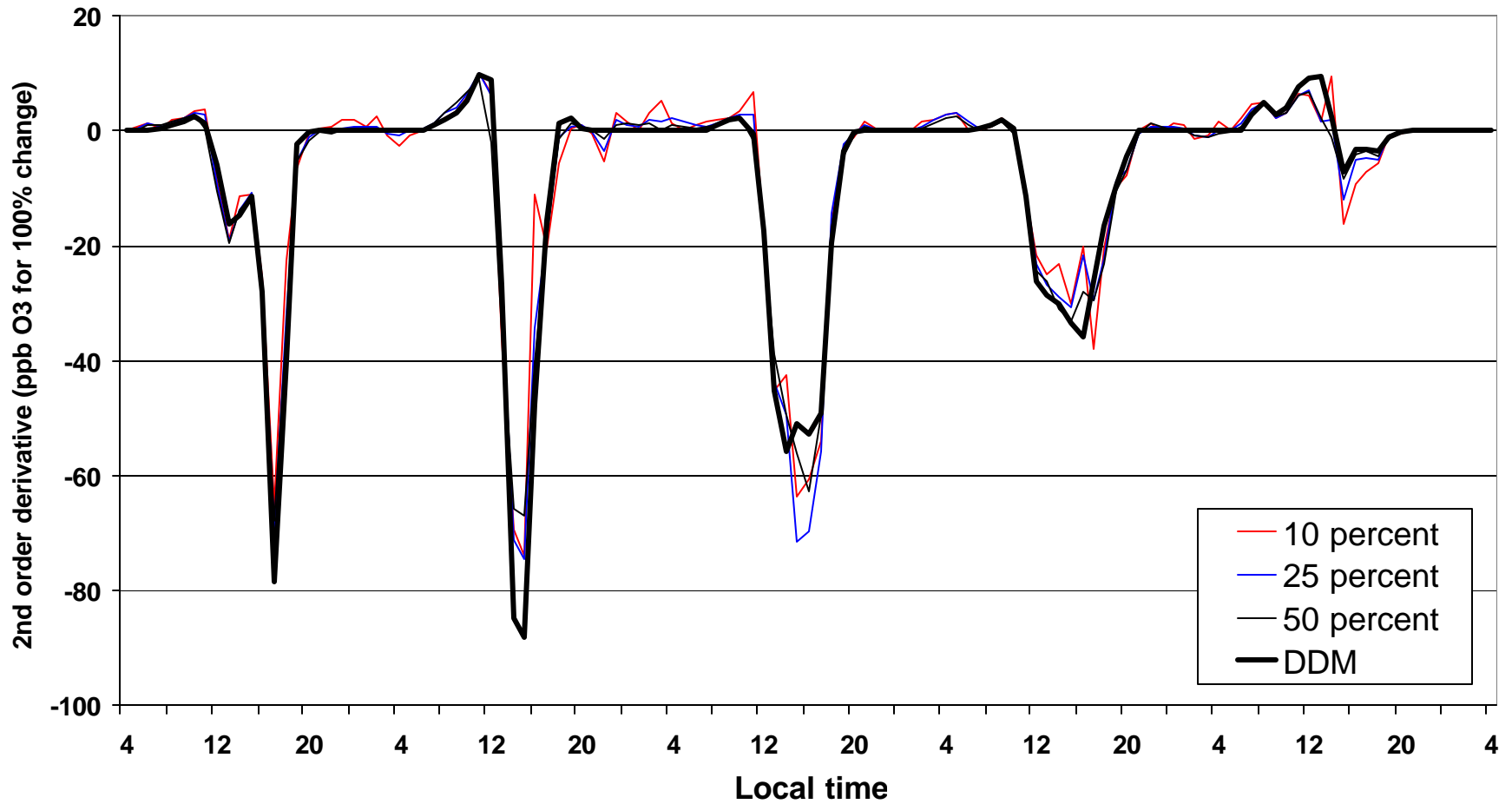


DDM vs. BF?

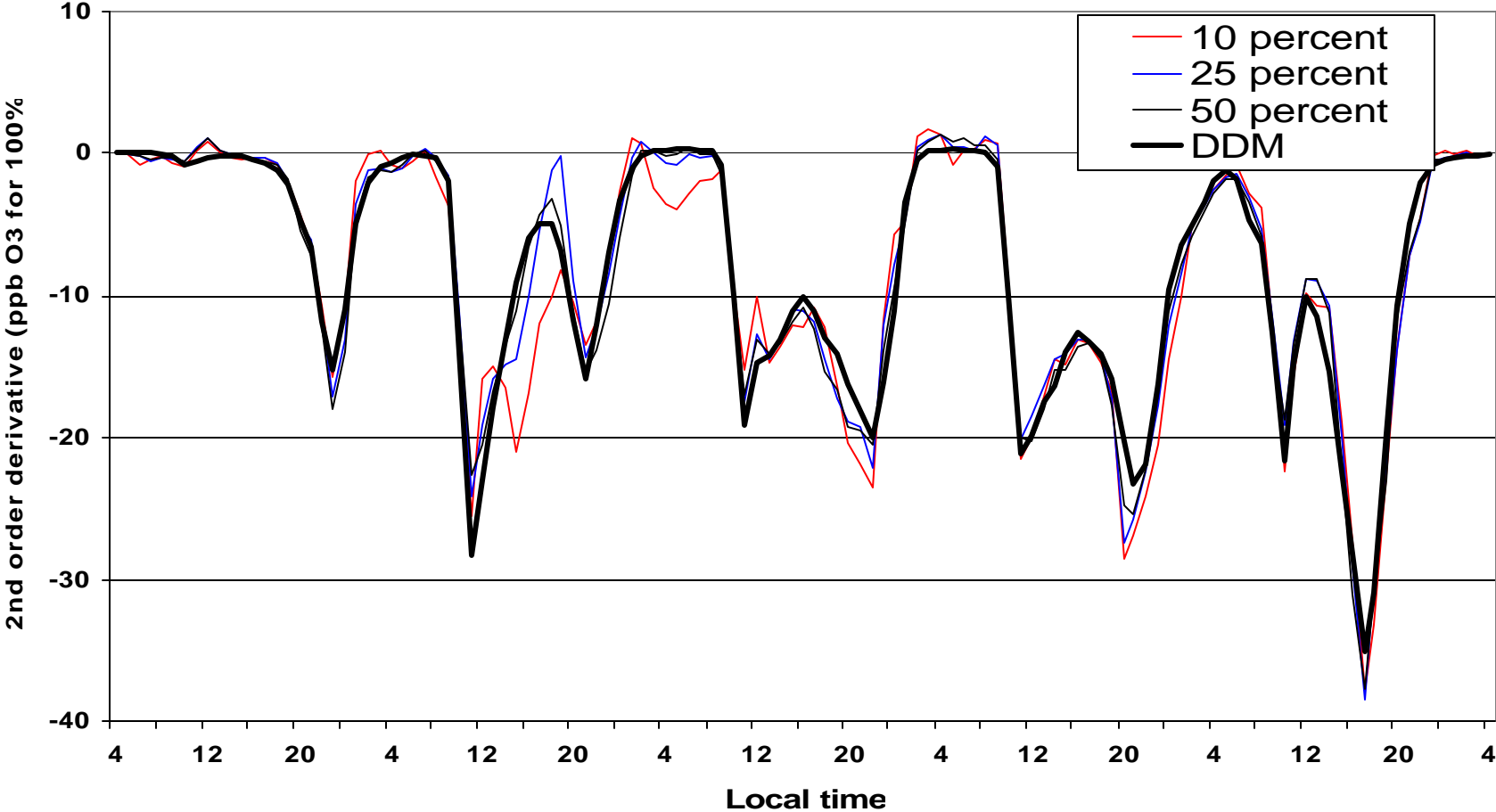
- A concave ozone response at high ozone concentration is unlikely.



DDM vs. BF 2nd order derivative: VOC-limited



DDM vs. BF 2nd order derivative: NO_x-limited

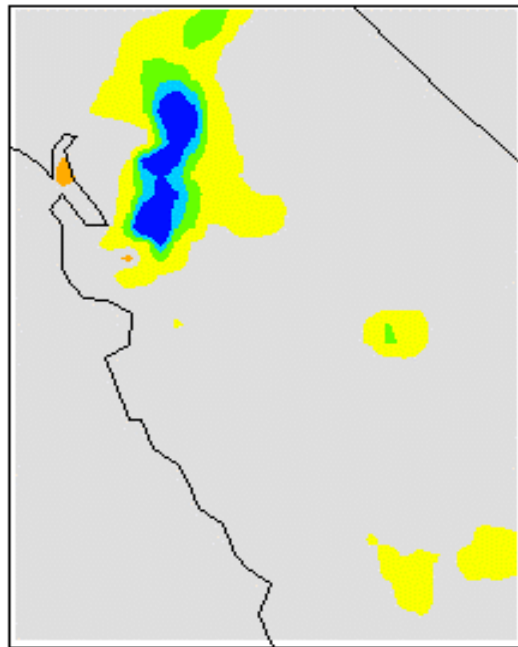


Non-linearity: where, why?



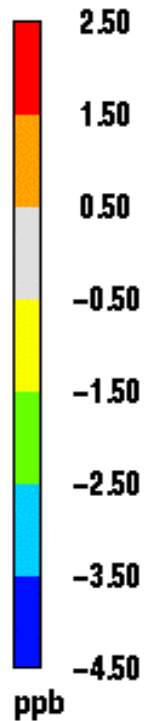
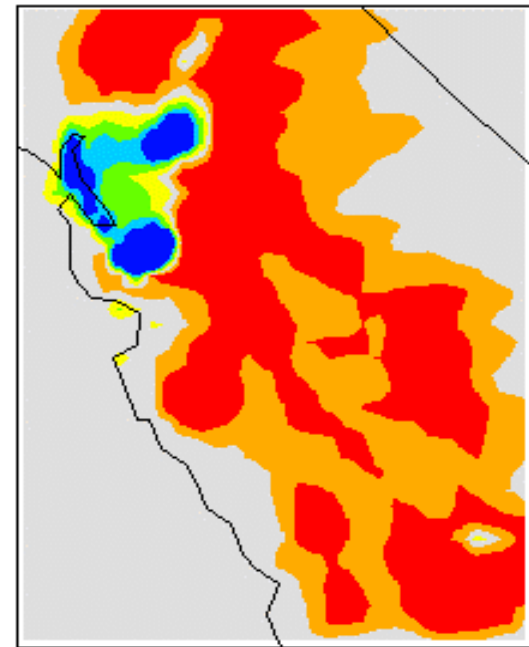
2nd order DDM

25% domain-wide NO
4 pm, local time

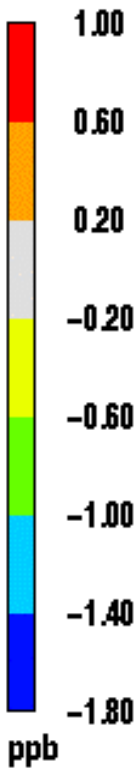


1st order DDM

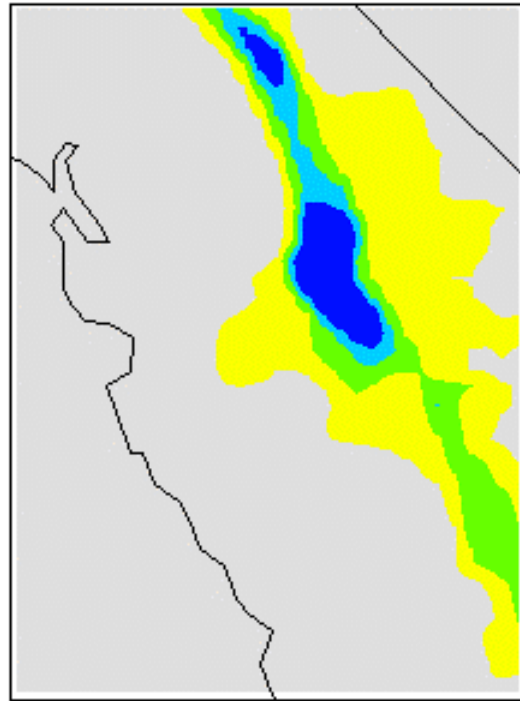
25% domain-wide NO
4 pm, local time



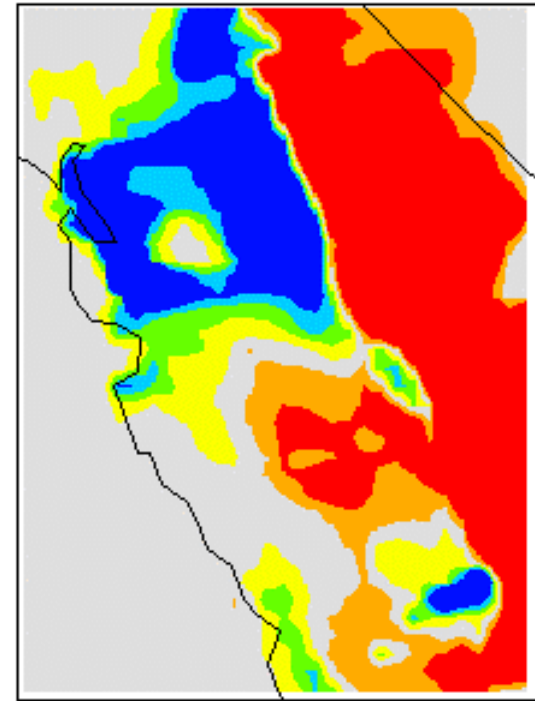
Non-linearity: where, why? (contd.)



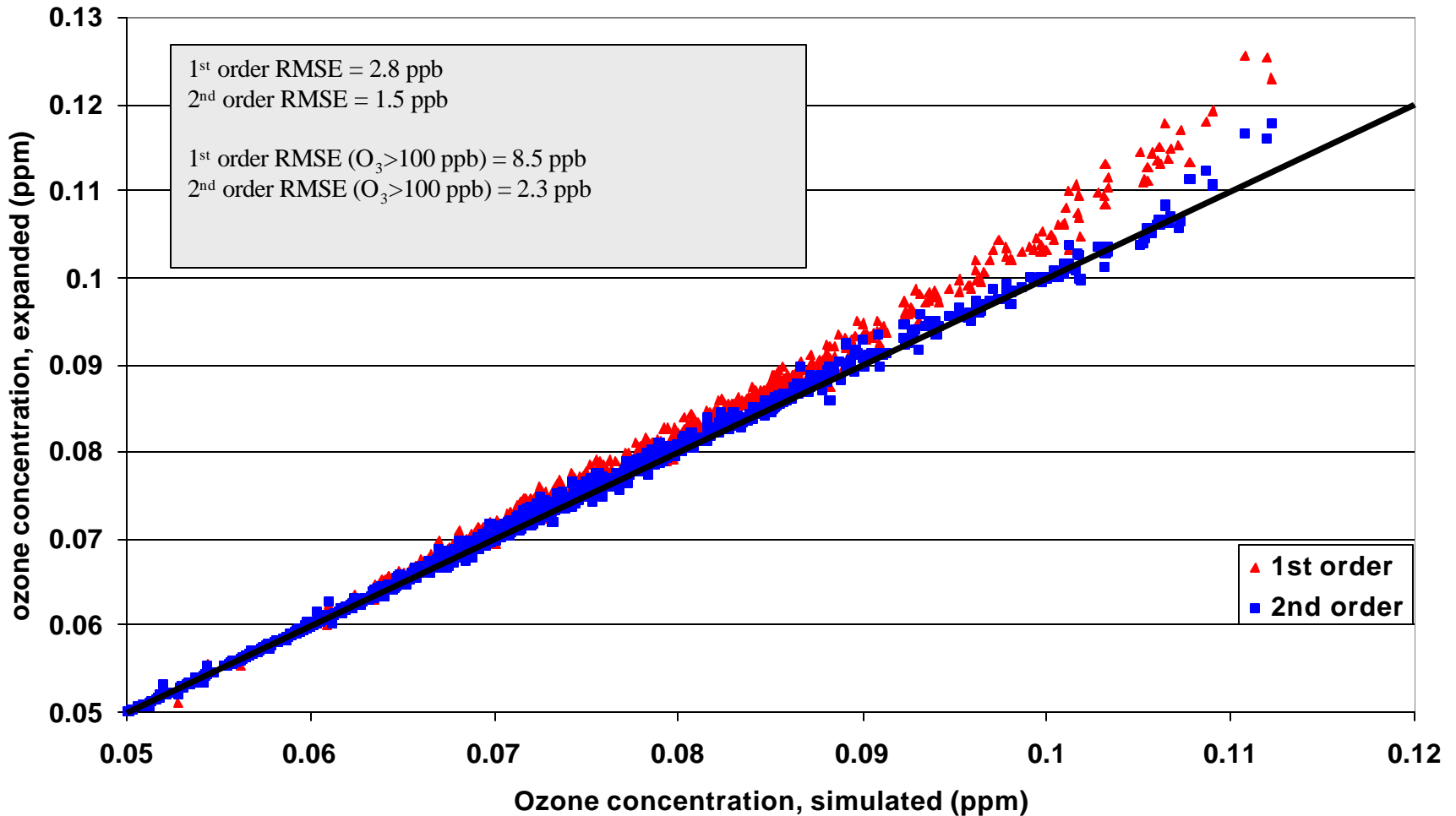
2nd order FDDM
10 PM, local time



1st order DDM
10 PM, local time



Non-linearity: where, why? (contd.)



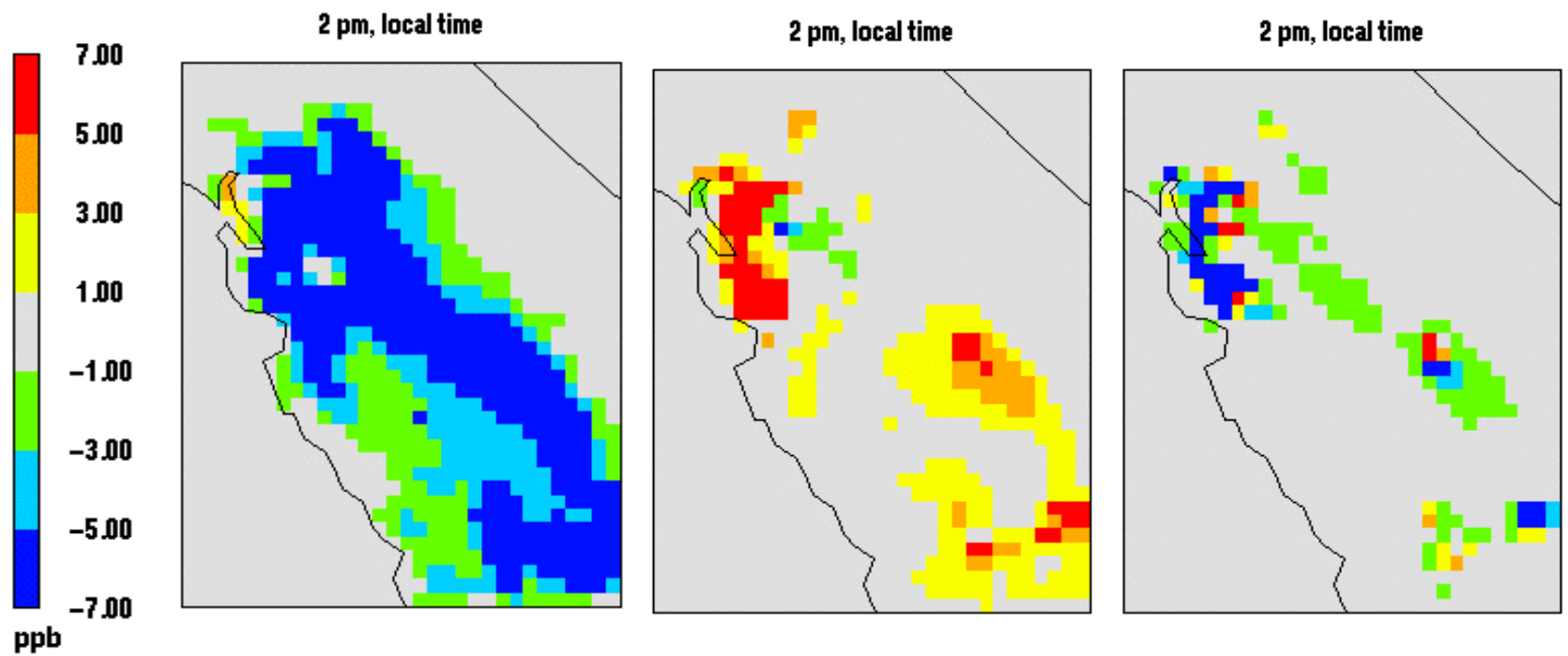
Higher order derivatives (domain-wide NO)



2nd order (NO) / 2

3rd order (NO) / 6

4th order (NO) / 24



Higher order derivatives (domain-wide VOC)

1st order (VOC)

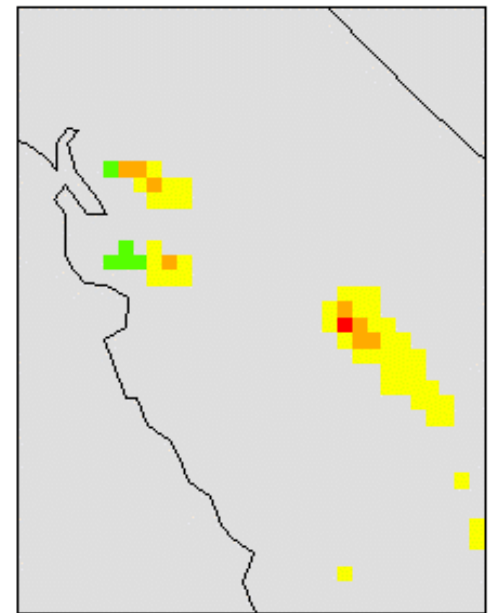
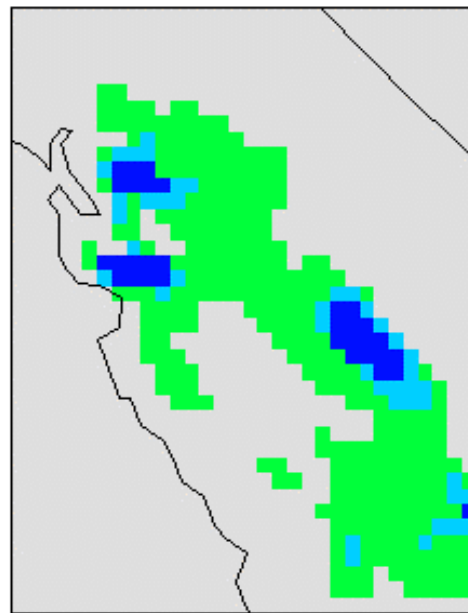
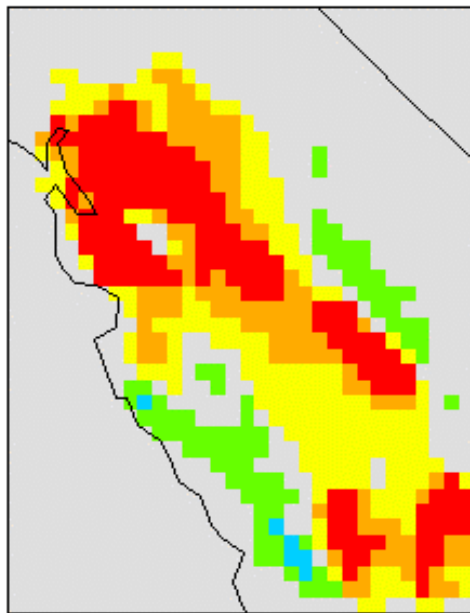
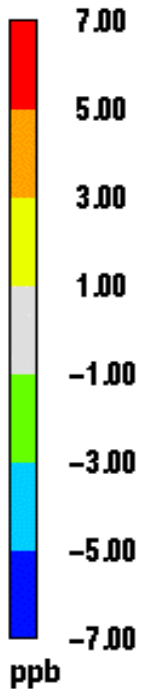
2nd(voc_voc)/2

3rd(voc_voc_voc)/6

2 pm, local time

2 pm, local time

2 pm, local time



Taylor series expansion

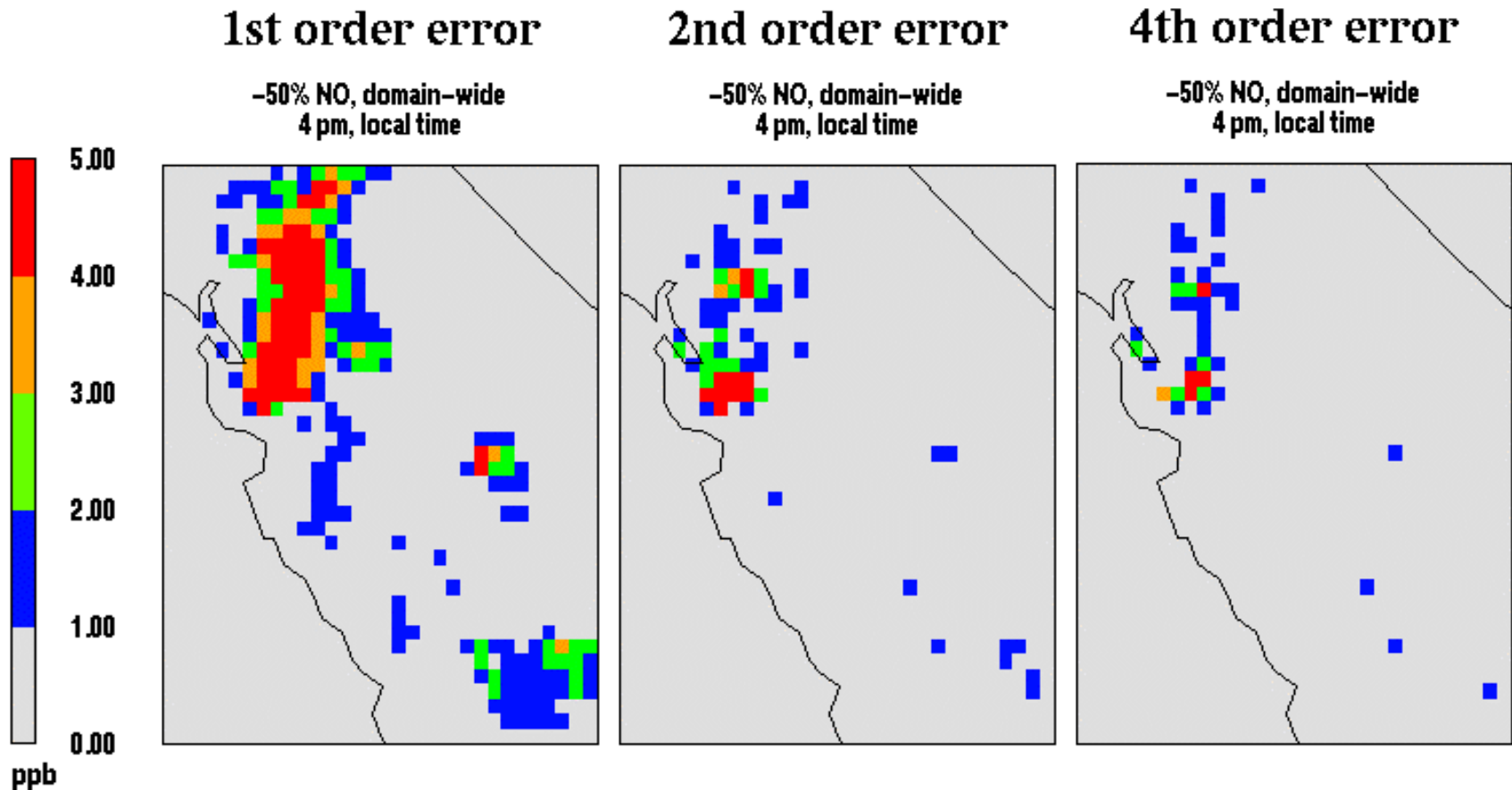


- One way to test the accuracy of the calculated derivatives:

$$C(x_0 + \Delta x) = C(x_0) + \Delta x S^{(1)}(x_0) + \frac{(\Delta x)^2}{2} S^{(2)}(x_0) \\ + \frac{(\Delta x)^3}{6} S^{(3)}(x_0) + \frac{(\Delta x)^4}{24} S^{(4)}(x_0) + \dots$$

- More accurate Taylor expansion:
 - Higher-order terms,
 - Smaller perturbation.
- Not the most accurate scaling method (Kramer et al., 1984)

Taylor series expansion: 50% reduction in NO



Taylor series expansion (contd.)



1st order error

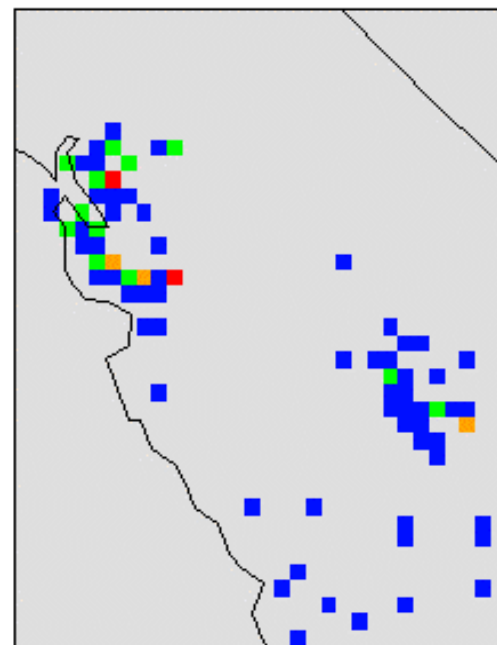
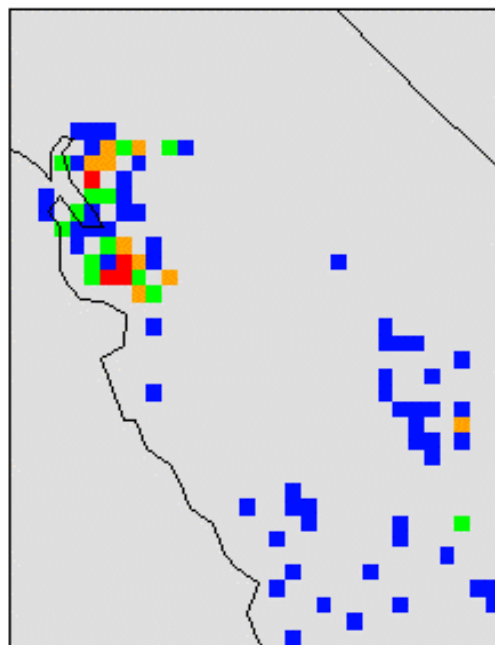
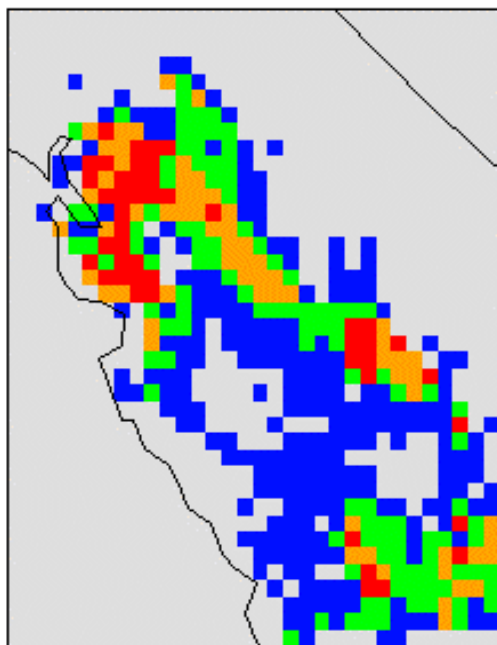
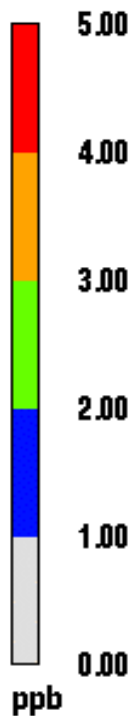
-50% NO, domain-wide
2 pm, local time

2nd order error

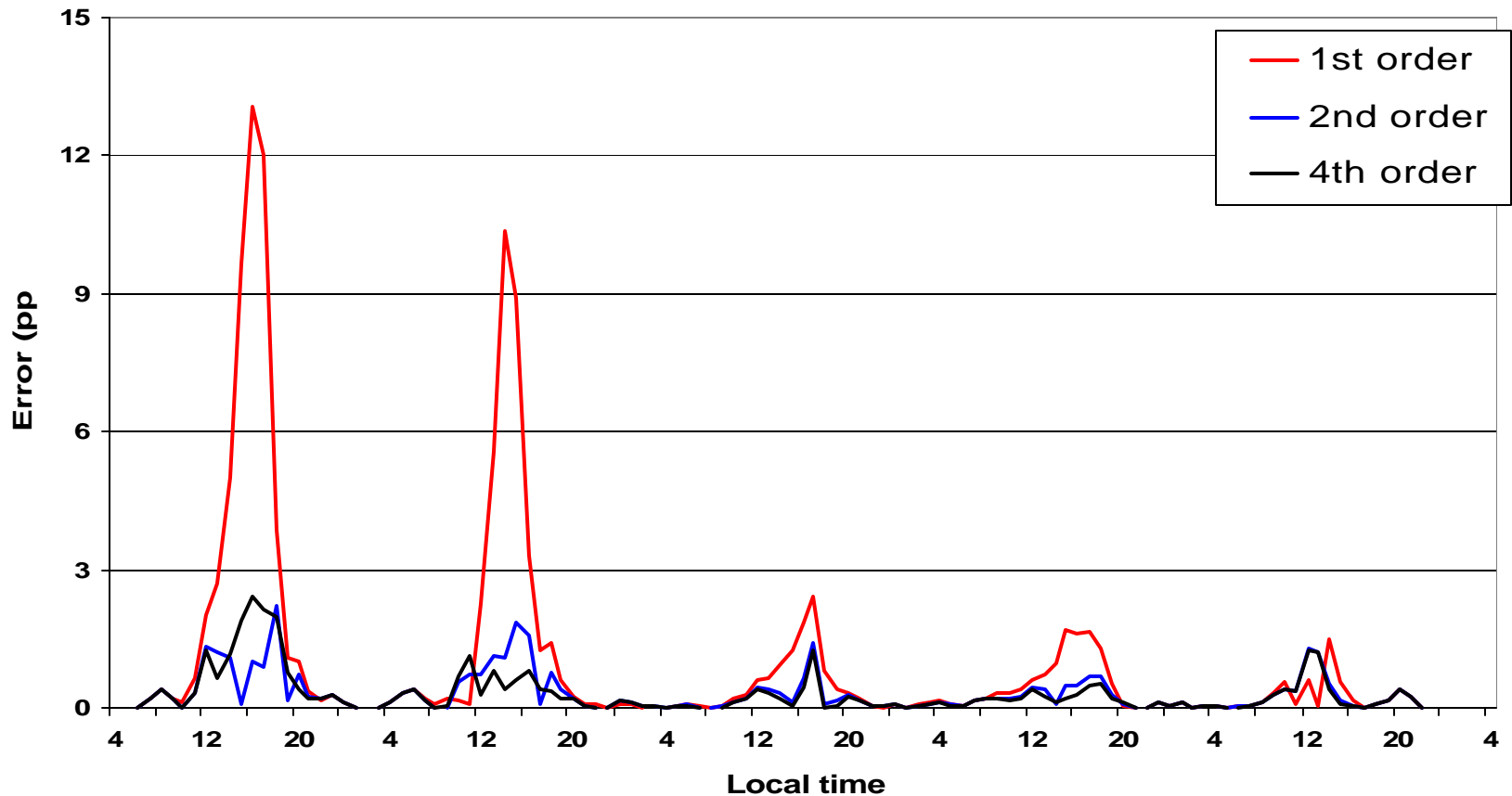
-50% NO, domain-wide
2 pm, local time

4th order error

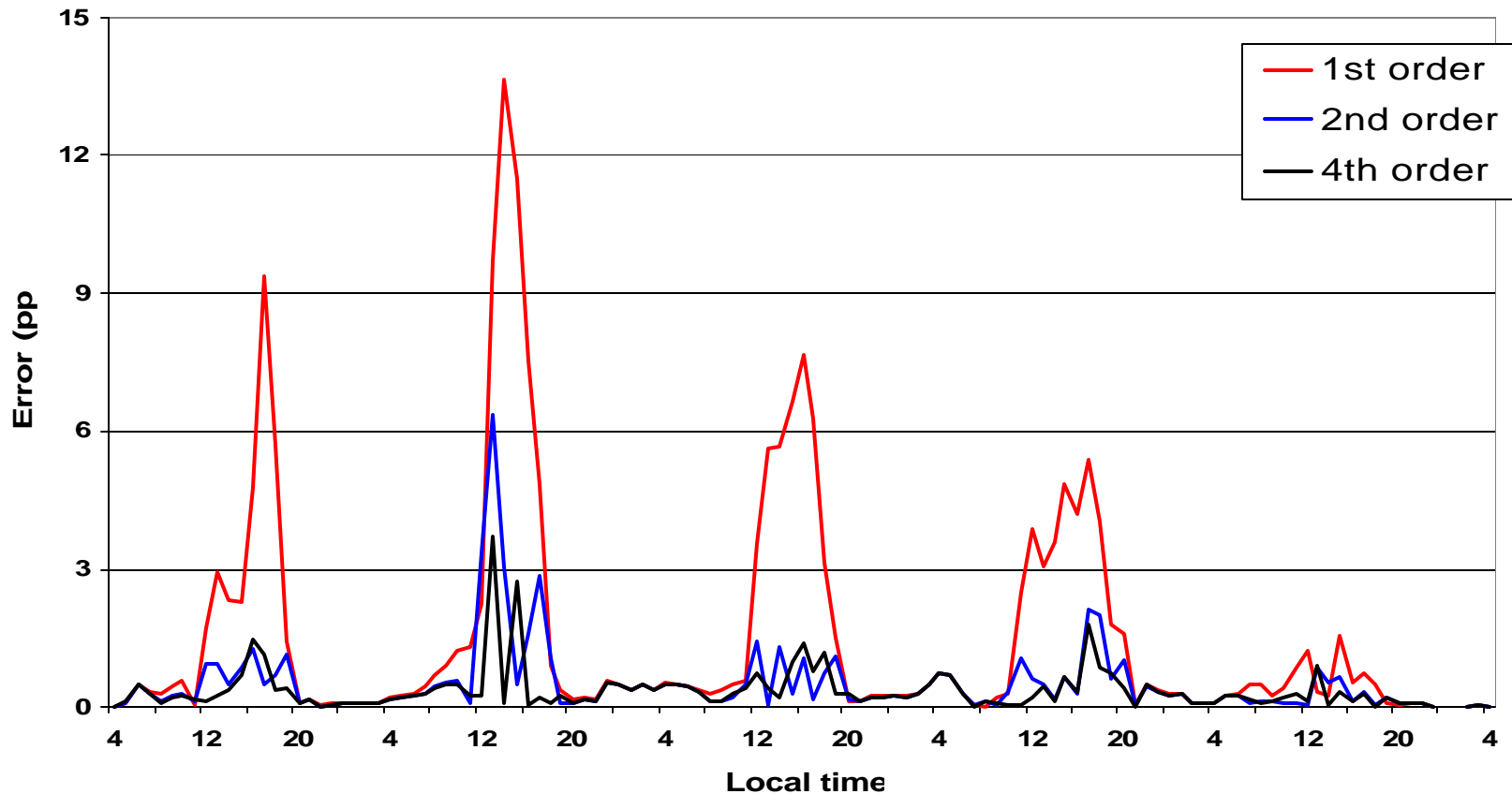
-50% NO, domain-wide
2 pm, local time



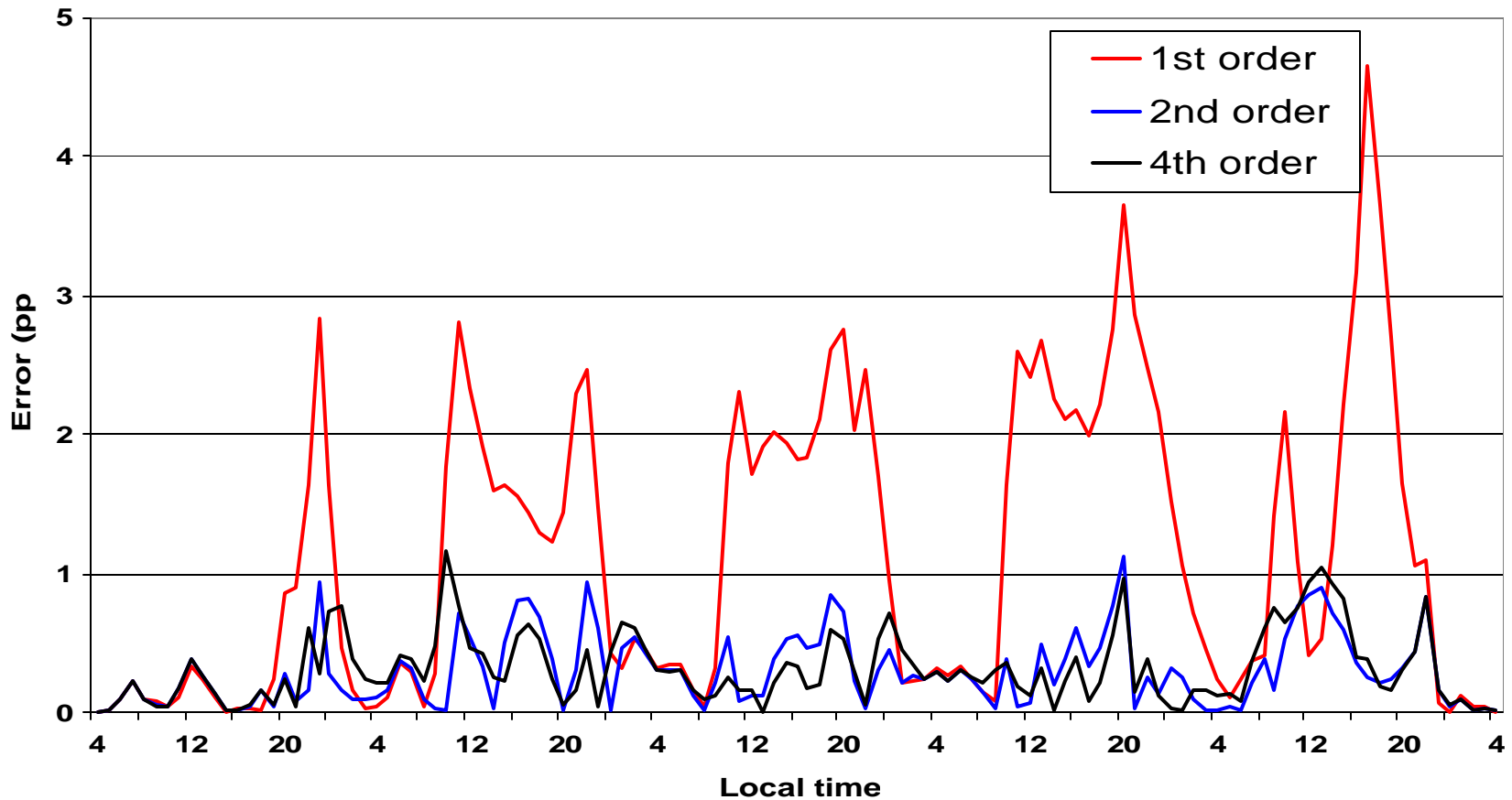
Taylor expansion: NO perturbation, location of the peak ozone



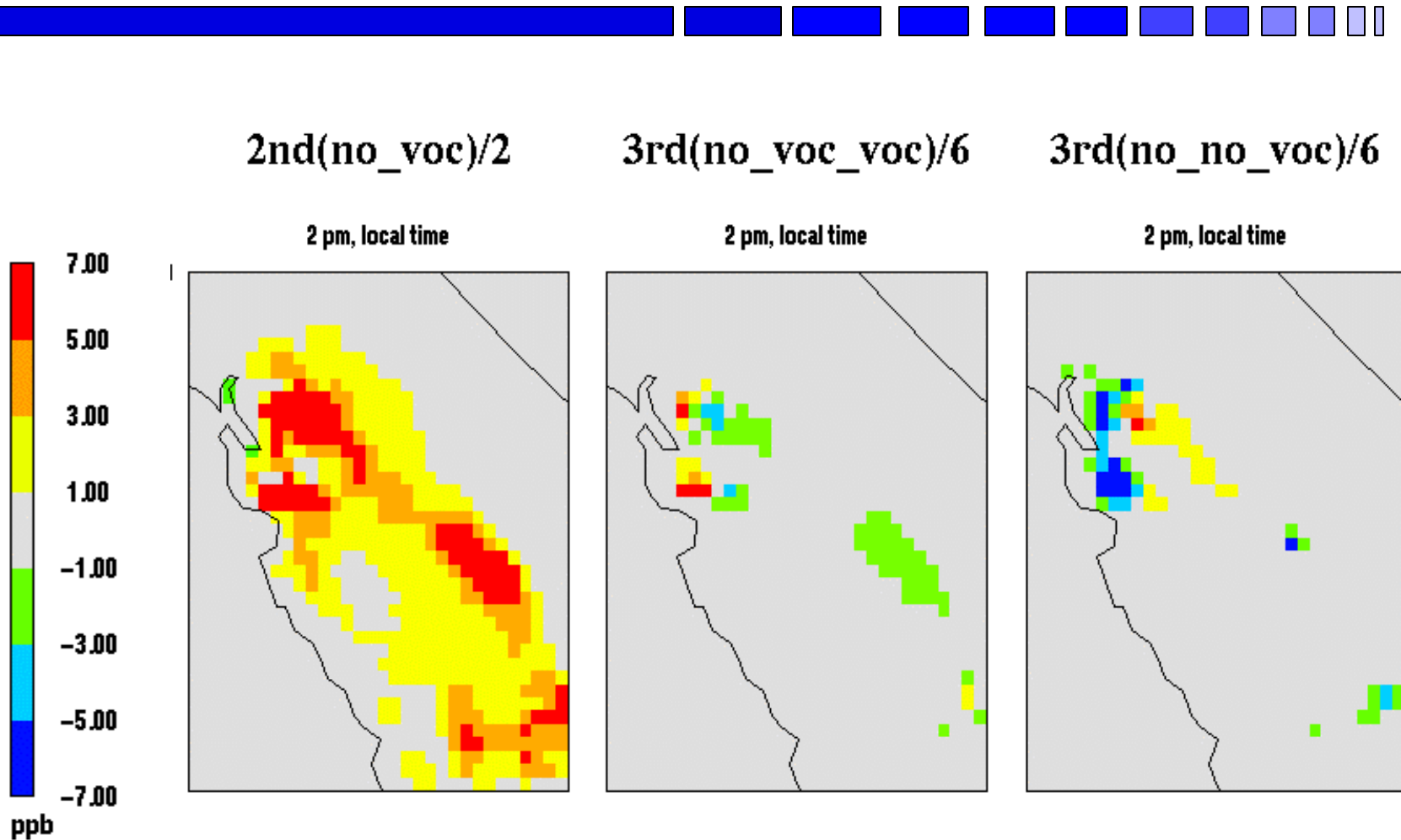
Taylor expansion: NO perturbation, VOC-limited



Taylor expansion: NO perturbation, NO_x-limited



Cross-derivatives (domain-wide NO/VOC)



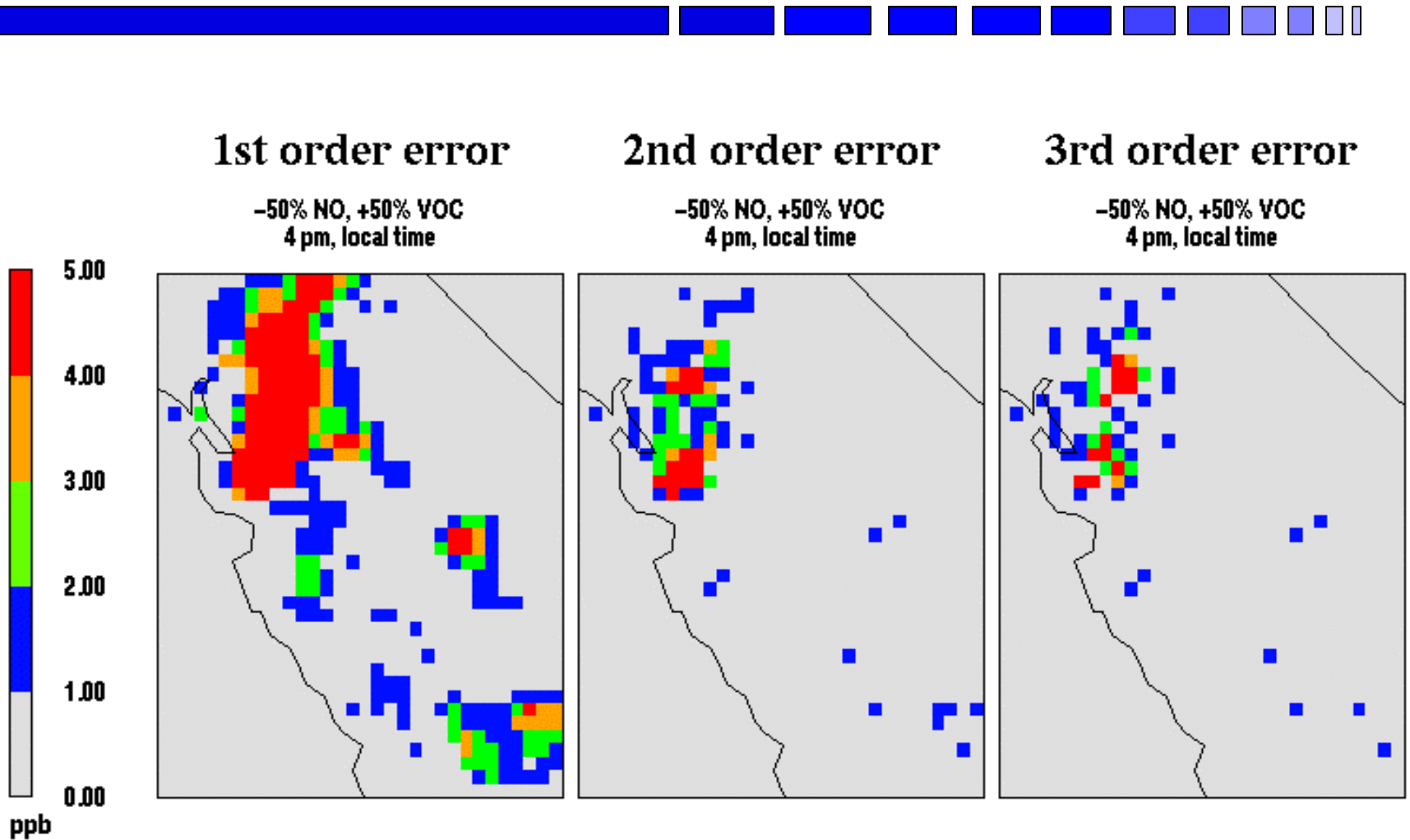
Taylor series expansion (contd.)



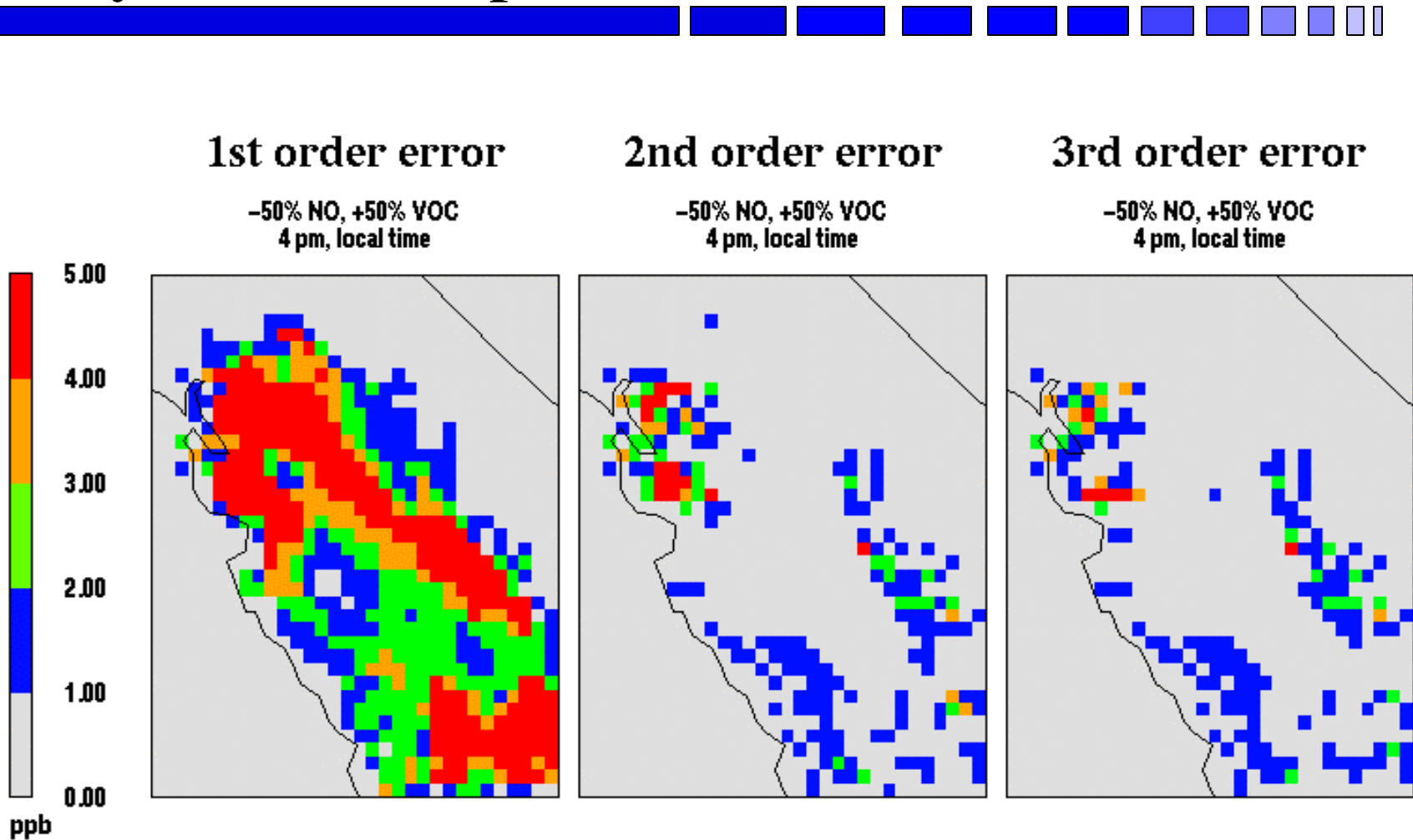
- For more than one sensitivity parameter:

$$\begin{aligned} C(x_0 + \Delta x, y_0 + \Delta y) = & C(x_0, y_0) + \Delta x S_x^{(1)}(x_0, y_0) + \Delta y S_y^{(1)}(x_0, y_0) \\ & + \frac{(\Delta x)^2}{2} S_{xx}^{(2)}(x_0, y_0) + (\Delta x)(\Delta y) S_{xy}^{(2)}(x_0, y_0) \\ & + \frac{(\Delta y)^2}{2} S_{yy}^{(2)}(x_0, y_0) + \frac{(\Delta x)^3}{6} S_{xxx}^{(3)}(x_0, y_0) \\ & + \frac{(\Delta x)^2(\Delta y)}{2} S_{xxy}^{(3)}(x_0, y_0) + \frac{(\Delta x)(\Delta y)^2}{2} S_{xyy}^{(3)}(x_0, y_0) \\ & + \frac{(\Delta y)^3}{6} S_{yyy}^{(3)}(x_0, y_0) + \dots \end{aligned}$$

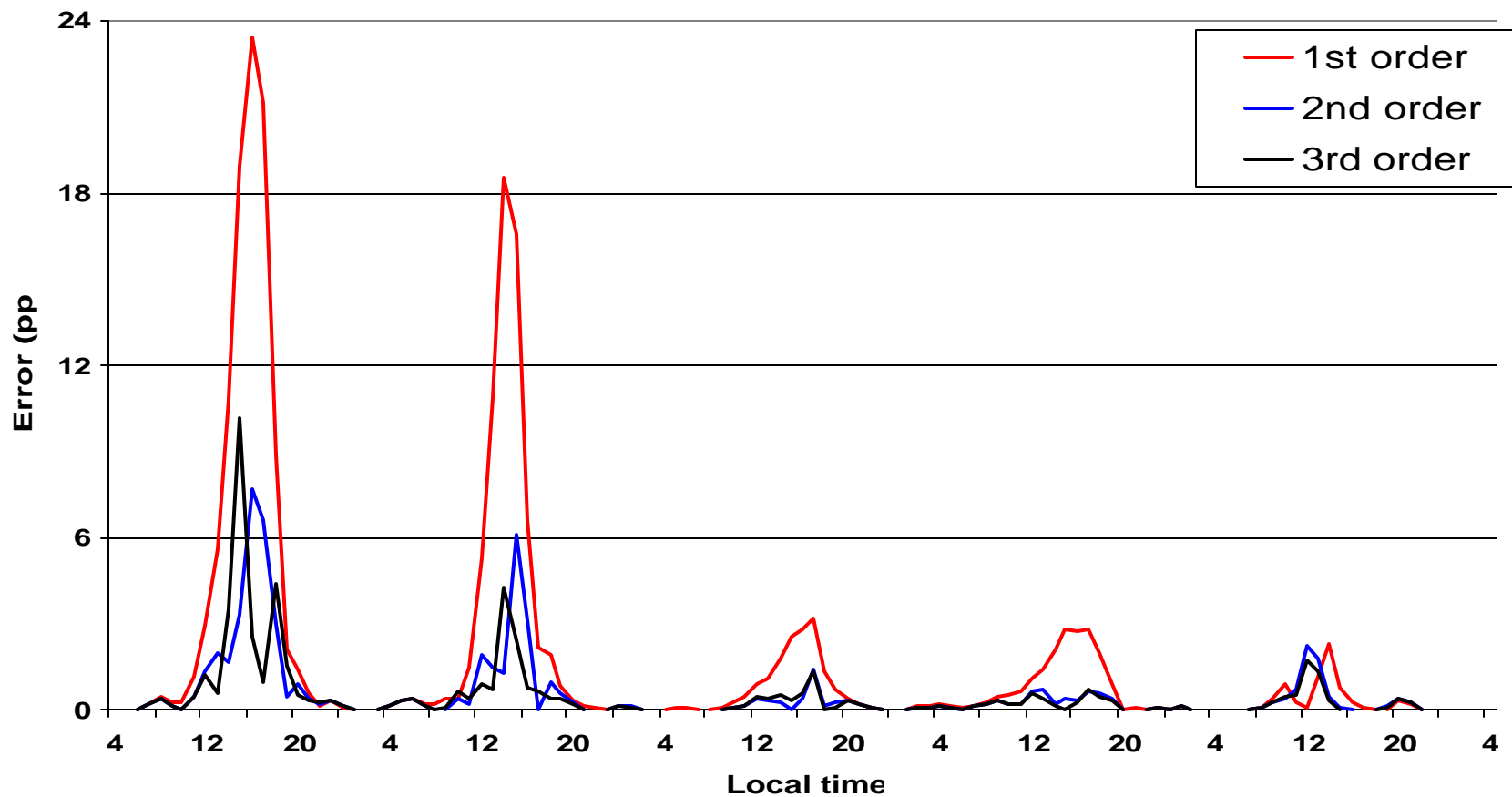
Taylor series expansion: combined perturbation



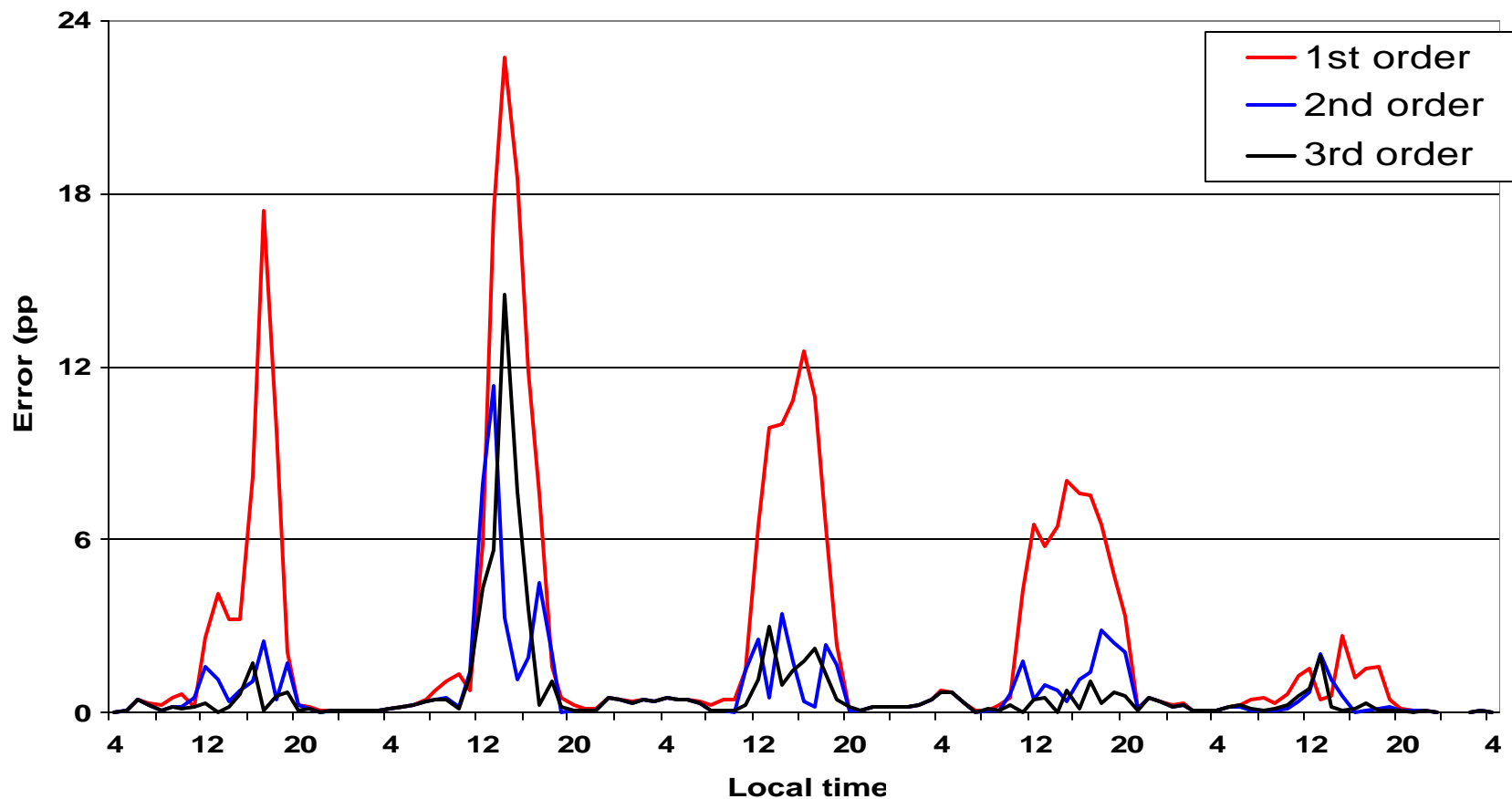
Taylor series expansion (contd.)



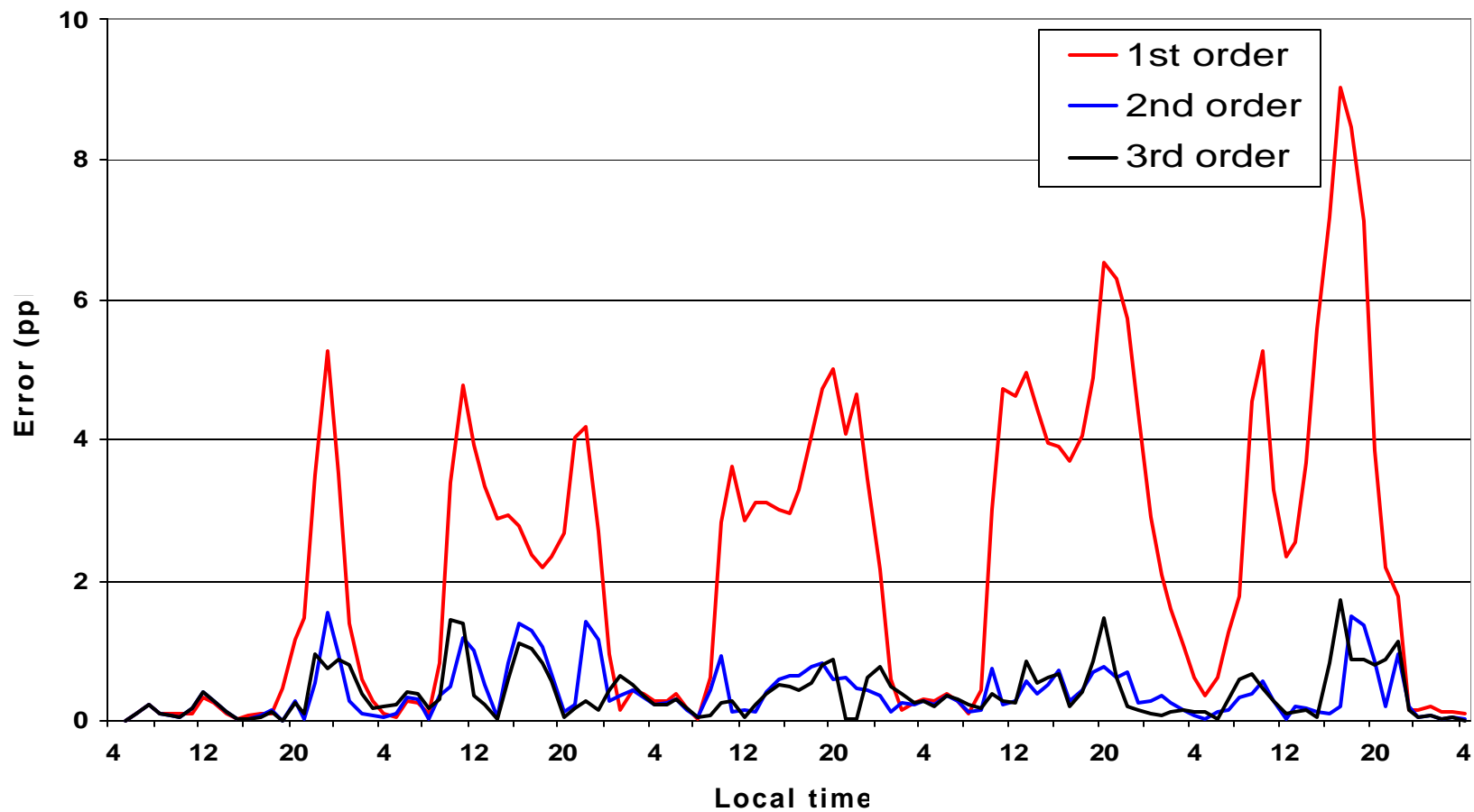
Taylor series expansion: NO/VOC perturbation, peak location



Taylor series expansion: NO/VOC perturbation, VOC-limited



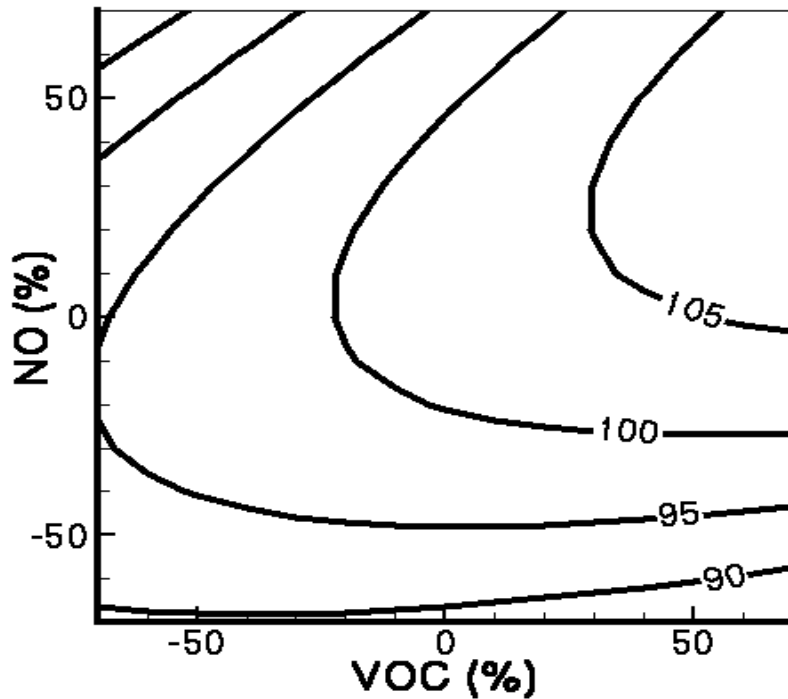
Taylor series expansion: NO/VOC perturbation, NO_x-limited



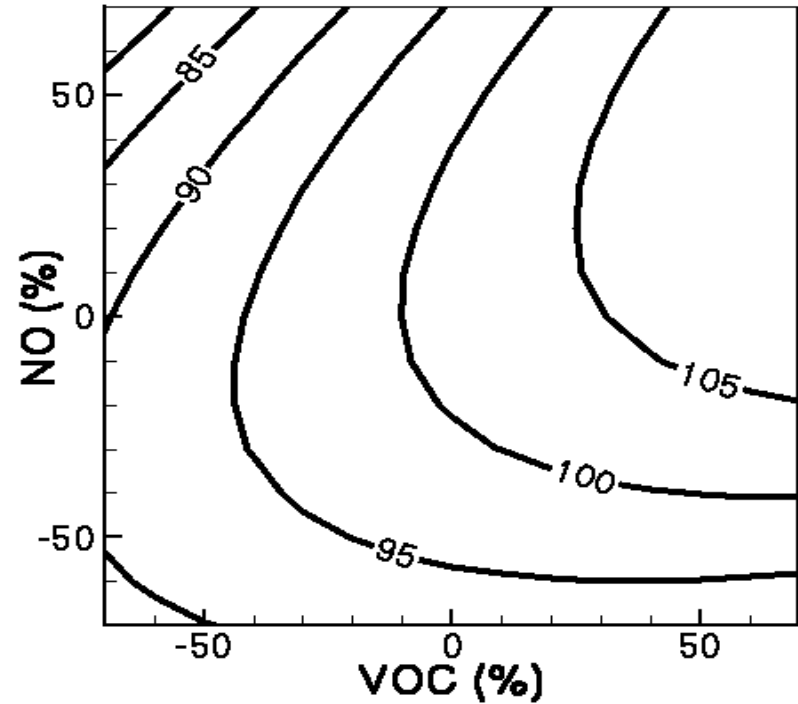
Ozone Isopleths (peak location), 2 PM



1st day



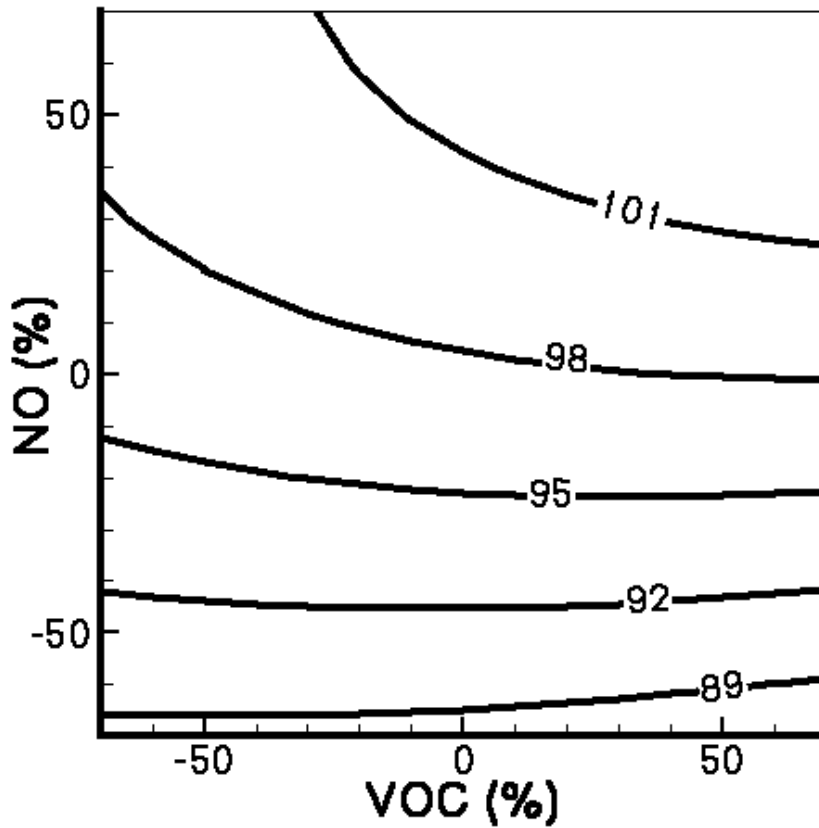
2nd day



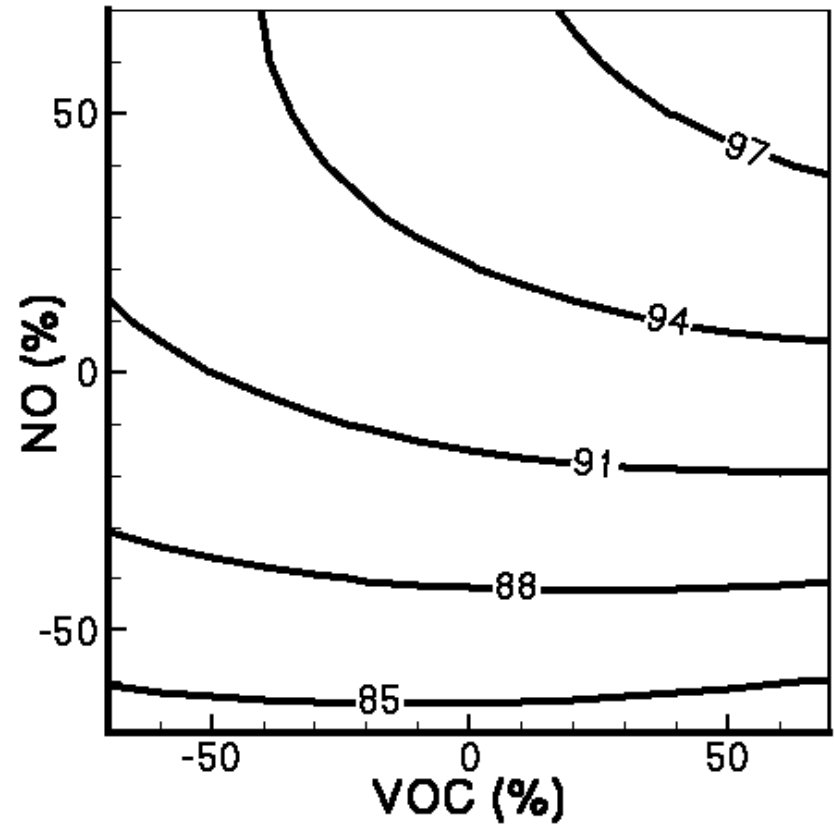
Ozone Isopleths (peak location), 2 PM (contd.)



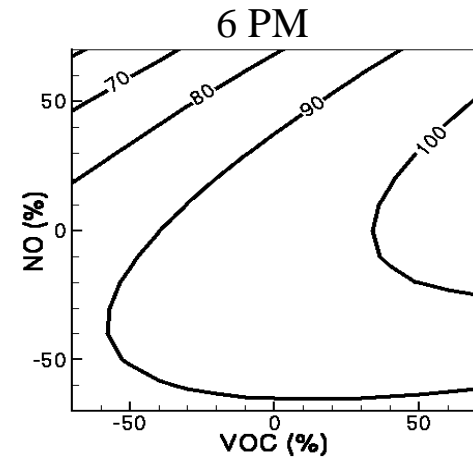
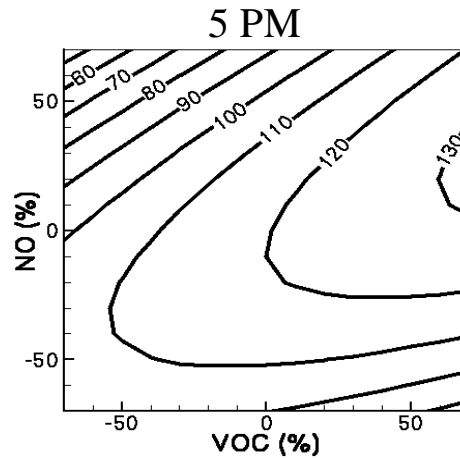
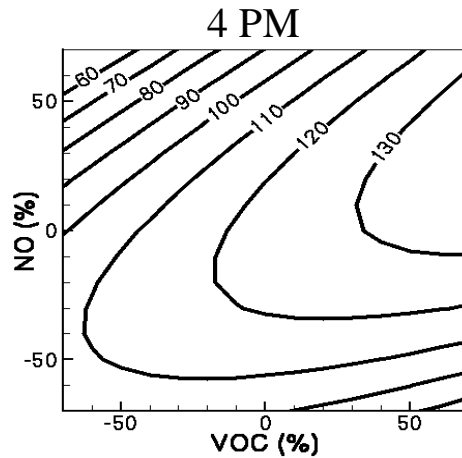
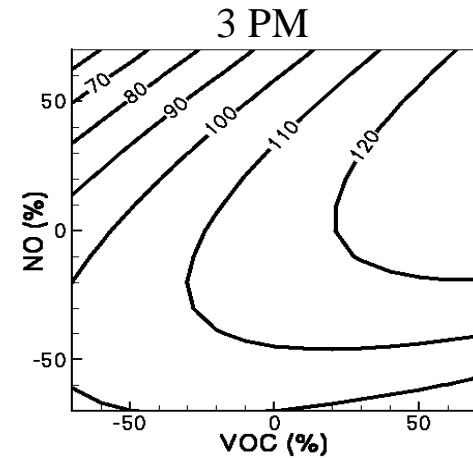
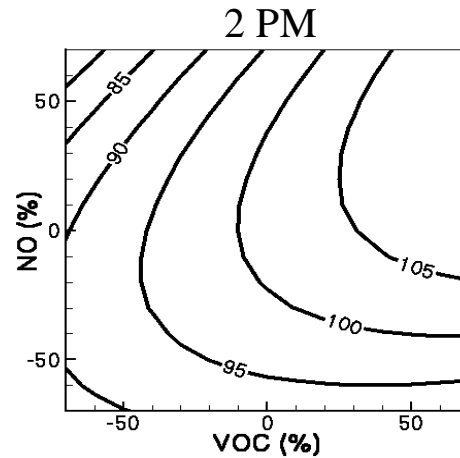
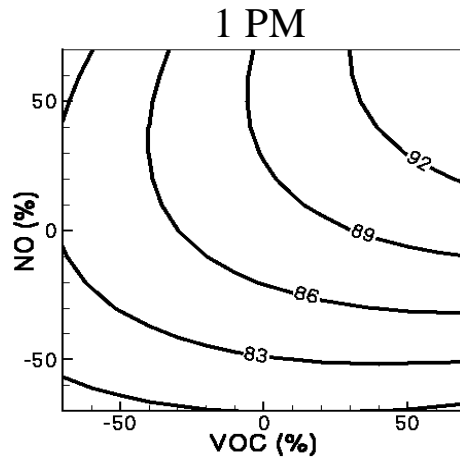
3rd day



4th day



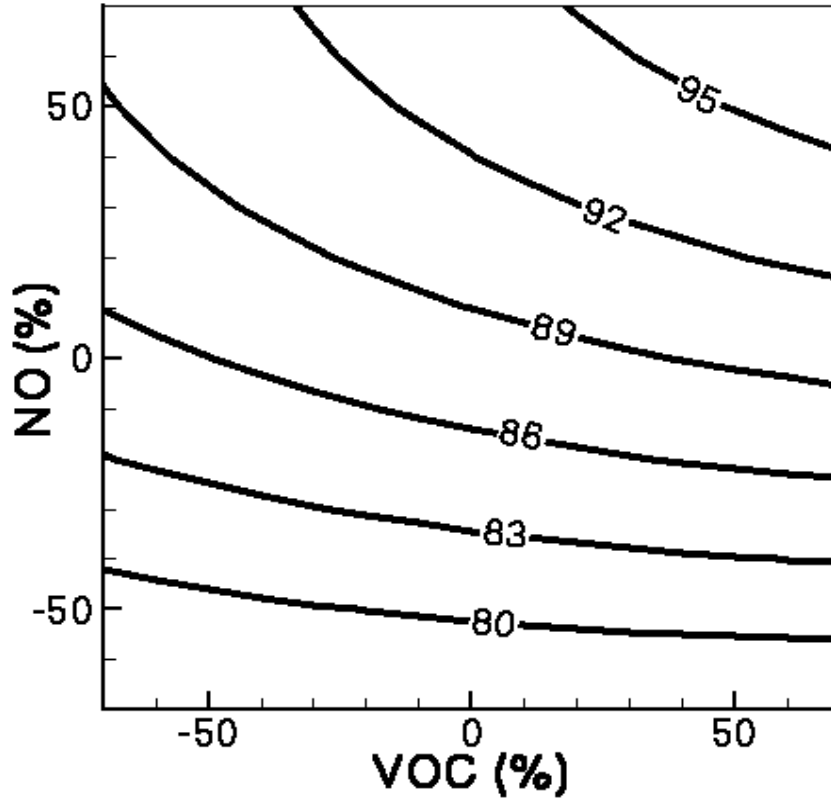
Ozone Isopleths, peak location (1-6 PM)



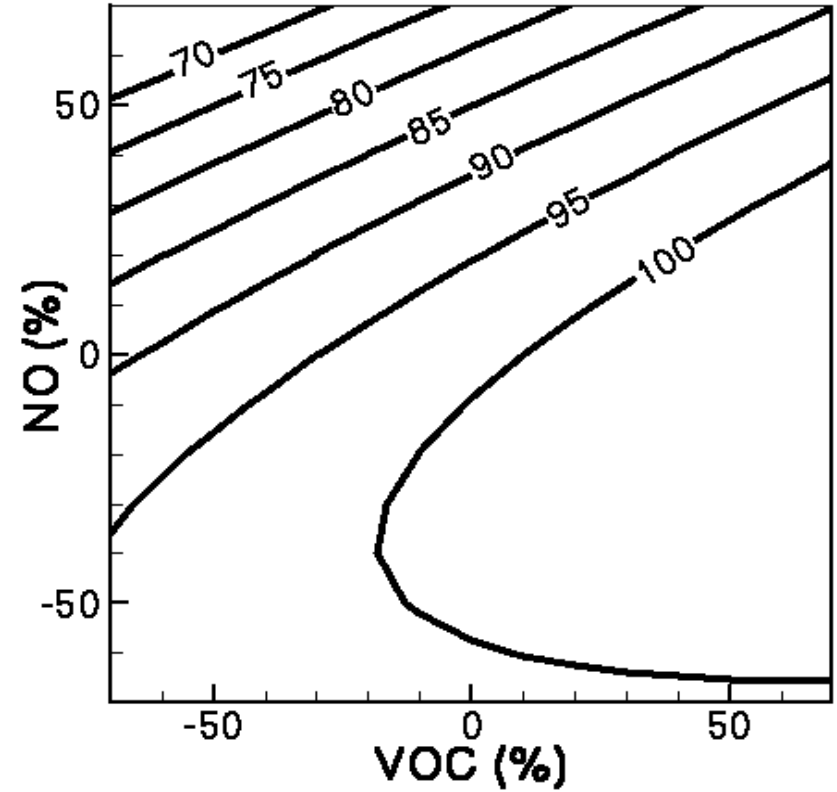
Ozone Isopleths, different regimes (2 PM)



NO_x-limited



VOC-limited




Summary



- HDDM provides an efficient tool for the calculation of high-order sensitivity coefficients.
- Higher-order sensitivity analysis can, to a large extent, explain the non-linearities in atmospheric response, e.g. ozone isopleths.
- Most of the improvement in accuracy is achieved by adding the 2nd order coefficients (curvature).
- Non-linear behavior in photochemistry usually happens at the time/location of a transition between different chemical regimes.
- The location and time of the peak ozone is usually subject to a high degree of non-linearity. This is potentially important for the case of NO_x control in an urban plume.

What should be done? What can be done?



- Higher-order sensitivity analysis is a completely unexplored territory. More research to come.
- Higher-order derivatives become unrealistically large -- should investigate the numerical limitations.
- Despite efficiency of HDDM, calculating higher derivatives of too many sensitivity parameters will be costly.
- HDDM provides us with new approach to old problems:
 - Cost-effectiveness analysis of control strategies,
 - Inverse modeling of non-linear systems,
 - Uncertainty analysis of organic reactivities,
 - And in general, description of any non-linearity, e.g. ozone isopleths.

Acknowledgement



- CARB
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